

PCT

NOTIFICATION OF ELECTION

(PCT Rule 61.2)

From the INTERNATIONAL BUREAU

To:

Commissioner
US Department of Commerce
United States Patent and Trademark
Office, PCT
2011 South Clark Place Room
CP2/5C24
Arlington, VA 22202
ETATS-UNIS D'AMERIQUE
in its capacity as elected Office

Date of mailing (day/month/year) 12 December 2000 (12.12.00)	Applicant's or agent's file reference 9023.21.WO
International application No. PCT/US00/05124	Priority date (day/month/year) 01 March 1999 (01.03.99)
International filing date (day/month/year) 29 February 2000 (29.02.00)	
Applicant SLEVA, Michael, Z. et al	

1. The designated Office is hereby notified of its election made:

☒ in the demand filed with the International Preliminary Examining Authority on:
18 September 2000 (18.09.00)

☐ in a notice effecting later election filed with the International Bureau on:

2. The election ☒ was
☐ was not

made before the expiration of 19 months from the priority date or, where Rule 32 applies, within the time limit under Rule 32.2(b).

The International Bureau of WIPO 34, chemin des Colombettes 1211 Geneva 20, Switzerland Facsimile No.: (41-22) 740.14.35	Authorized officer Claudio Borton Telephone No.: (41-22) 338.83.38
--	---

091.914682

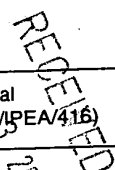
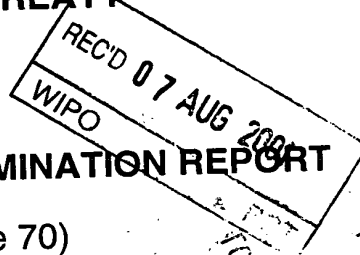
14

PATENT COOPERATION TREATY

PCT

INTERNATIONAL PRELIMINARY EXAMINATION REPORT

(PCT Article 36 and Rule 70)



Applicant's or agent's file reference 9023.21.WO	FOR FURTHER ACTION See Notification of Transmittal of International Preliminary Examination Report (Form PCT/IPEA/416)	
International application No. PCT/US00/05124	International filing date (day/month/year) 29/02/2000	Priority date (day/month/year) 01/03/1999
International Patent Classification (IPC) or national classification and IPC B06B1/06		
Applicant MEDACOUSTICS, INC. et al.		

1. This international preliminary examination report has been prepared by this International Preliminary Examining Authority and is transmitted to the applicant according to Article 36.


2. This REPORT consists of a total of 16 sheets, including this cover sheet.

- ☐ This report is also accompanied by ANNEXES, i.e. sheets of the description, claims and/or drawings which have been amended and are the basis for this report and/or sheets containing rectifications made before this Authority (see Rule 70.16 and Section 607 of the Administrative Instructions under the PCT).

These annexes consist of a total of sheets.

3. This report contains indications relating to the following items:

- I ☒ Basis of the report
- II ☐ Priority
- III ☒ Non-establishment of opinion with regard to novelty, inventive step and industrial applicability
- IV ☒ Lack of unity of invention
- V ☒ Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement
- VI ☐ Certain documents cited
- VII ☒ Certain defects in the international application
- VIII ☒ Certain observations on the international application

Date of submission of the demand 18/09/2000	Date of completion of this report 28.06.2001
Name and mailing address of the international preliminary examining authority:  European Patent Office D-80298 Munich Tel. +49 89 2399 - 0 Tx: 523656 epmu d Fax: +49 89 2399 - 4465	Authorized officer Tasiaux, B Telephone No. +49 89 2399 2555



INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No. PCT/US00/05124

I. Basis of the report

1. With regard to the **elements** of the international application (*Replacement sheets which have been furnished to the receiving Office in response to an invitation under Article 14 are referred to in this report as "originally filed" and are not annexed to this report since they do not contain amendments (Rules 70.16 and 70.17)*):

Description, pages:

1-43 as originally filed

Claims, No.:

1-73 as originally filed

Drawings, sheets:

1-30 as originally filed

2. With regard to the **language**, all the elements marked above were available or furnished to this Authority in the language in which the international application was filed, unless otherwise indicated under this item.

These elements were available or furnished to this Authority in the following language: , which is:

- ☐ the language of a translation furnished for the purposes of the international search (under Rule 23.1(b)).
- ☐ the language of publication of the international application (under Rule 48.3(b)).
- ☐ the language of a translation furnished for the purposes of international preliminary examination (under Rule 55.2 and/or 55.3).

3. With regard to any **nucleotide and/or amino acid sequence** disclosed in the international application, the international preliminary examination was carried out on the basis of the sequence listing:

- ☐ contained in the international application in written form.
- ☐ filed together with the international application in computer readable form.
- ☐ furnished subsequently to this Authority in written form.
- ☐ furnished subsequently to this Authority in computer readable form.
- ☐ The statement that the subsequently furnished written sequence listing does not go beyond the disclosure in the international application as filed has been furnished.
- ☐ The statement that the information recorded in computer readable form is identical to the written sequence listing has been furnished.

4. The amendments have resulted in the cancellation of:

- ☐ the description, pages:
- ☐ the claims, Nos.:

INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No. PCT/US00/05124

☐ the drawings, sheets:

5. ☐ This report has been established as if (some of) the amendments had not been made, since they have been considered to go beyond the disclosure as filed (Rule 70.2(c)):

(Any replacement sheet containing such amendments must be referred to under item 1 and annexed to this report.)

6. Additional observations, if necessary:

III. Non-establishment of opinion with regard to novelty, inventive step and industrial applicability

1. The questions whether the claimed invention appears to be novel, to involve an inventive step (to be non-obvious), or to be industrially applicable have not been examined in respect of:

☐ the entire international application.

☒ claims Nos. 46,57-65.

because:

☐ the said international application, or the said claims Nos. relate to the following subject matter which does not require an international preliminary examination (*specify*):

☒ the description, claims or drawings (*indicate particular elements below*) or said claims Nos. are so unclear that no meaningful opinion could be formed (*specify*):
see separate sheet

☐ the claims, or said claims Nos. are so inadequately supported by the description that no meaningful opinion could be formed.

☐ no international search report has been established for the said claims Nos. .

2. A meaningful international preliminary examination cannot be carried out due to the failure of the nucleotide and/or amino acid sequence listing to comply with the standard provided for in Annex C of the Administrative Instructions:

☐ the written form has not been furnished or does not comply with the standard.

☐ the computer readable form has not been furnished or does not comply with the standard.

IV. Lack of unity of invention

1. In response to the invitation to restrict or pay additional fees the applicant has:

☐ restricted the claims.

INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No. PCT/US00/05124

- ☒ paid additional fees.
- ☐ paid additional fees under protest.
- ☐ neither restricted nor paid additional fees.
2. ☐ This Authority found that the requirement of unity of invention is not complied and chose, according to Rule 68.1, not to invite the applicant to restrict or pay additional fees.
3. This Authority considers that the requirement of unity of invention in accordance with Rules 13.1, 13.2 and 13.3 is
- ☐ complied with.
- ☐ not complied with for the following reasons:
4. Consequently, the following parts of the international application were the subject of international preliminary examination in establishing this report:
- ☒ all parts.
- ☐ the parts relating to claims Nos. .

V. Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement

1. Statement

Novelty (N)	Yes:	Claims	2-17,26-43;51-56,66-67;70-73
	No:	Claims	1;18-21,23-25;45,47,49
Inventive step (IS)	Yes:	Claims	2-17,26-43;54;70-73
	No:	Claims	22;44;48,50-53,55-56,66-67,68-69
Industrial applicability (IA)	Yes:	Claims	1-73
	No:	Claims	

2. Citations and explanations see separate sheet

VII. Certain defects in the international application

The following defects in the form or contents of the international application have been noted:
see separate sheet

VIII. Certain observations on the international application

The following observations on the clarity of the claims, description, and drawings or on the question whether the claims are fully supported by the description, are made:

**INTERNATIONAL PRELIMINARY
EXAMINATION REPORT**

International application No. PCT/US00/05124

see separate sheet

Re Item III

Non-establishment of opinion with regard to novelty, inventive step and industrial applicability

See sections VIII.2.1 and VIII.3.1.

Re Item IV

Lack of unity of invention

Cf. Form 405, sections 1 to 9.

Re Item V

Reasoned statement under Rule 66.2(a)(ii) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement

1. Claims 1-44

Claim 1 : From a structural point of view, Claim 1 reduces to a set of "acoustic" strips with one or more sensor elements on it.

Such a sensor array is disclosed by US-A- 5 807 271, hereinafter referred to as D12, see in particular Fig. 3 as well as the corresponding description.

Claims 18-21, 23-25 : a sensor element with the very same features as the ones listed in Claims 18-25 is known from WO-A- 98 22786, hereinafter referred to as D11, see in particular Fig. 1 to 4 as well as the corresponding description.

Indeed, the known sensor element is made of a flexible elastomeric core material 16 (having a thickness between 381 and 1524 μm , see pg. 6, l. 29) sandwiched between two piezoelectric layers 12 and 14 of PVDF (see pg. 5, l. 6 ; having a thickness between 20 and 60 μm , see pg. 6, l. 29)), each having an active electrode 32 facing the elastomeric (pg. 6, l. 18) core and a ground electrode 22 on the respective outer surface. As in the present case, this structure allows to generate two distinct voltage signals having opposite polarities, see Fig. 4, which are amplified by a differential amplifier to obtain the output signal, see pg. 6, 1st §.

Claim 22 : this structural detail is not explicitly disclosed by D11. However, it does not produce any unexpected effect.

Claim 44 : is obvious from the combination of D12 and D11. Indeed, using the sensor elements of D11 with the belt shown in D12 is already known the measure fetal heartbeat. However, it is obvious that the heartbeat of a fully-grown patient could be measured as well with the same hardware.

Positive Hint :

1. Linking the sensor elements along a strip by a frame as shown in Fig. 5 of the present application (all sensor linked to a single frame leg) or in Fig. 6 (alternate side link along two parallel frame legs).

It is therefore advised to the applicant to drop the independent claim defining solely the sensor element and to focus on the sensor array. If an independent claim defining solely the sensor element is kept, the claim structure should take into account the comments made in Section VIII.1.1.

2. In this respect, the features described in the apparatus claims 2-17 and 26-36 appear to involve some inventive matter. However, it is unclear at this stage, which features will be used to define the subject-matter of an independent claim including all features necessary to solve the stated problem, see Section VIII.1 and in particular Section VIII.1.12.
3. The features disclosed in the method Claims 37-43 are also novel and inventive inasmuch as the independent method claim would include an *explicit* reference to an independent apparatus that would take into account the remarks of the previous paragraph.

2. Claims 45-56, 66-67, 68-69

Claims 45, 47 and 49 : the subject-matter of these claims is known from Document US-A- 5 795 299, hereinafter referred to as D21, see in particular Fig. 1-3 and 10 as well as the corresponding description, describes a sensor array presenting the same

structural features as the sensor array defined by the aforementioned claims.

D21 discloses a sensor array (20) with a plurality of acoustic sensor elements (26, cf. col. 2, l. 58) and a plurality of transmission lines (35) having opposing first near 38, Fig. 3) and second (40) ends, the first end being individually attached to an acoustic sensor element (cf. col. 3, 2nd §, in particular l. 8-10), the second end being connected to a connector (40 ; Fig. 3) receiving a portion of the transmission line (see also Fig. 19), said transmission lines being configured with a series of undulation along its length (see Fig. 10).

Claims 48 and 50 appears to describe generic features of a transducer array having separated elements. Such transducer elements are know per se as well as their generic properties and structure, see by example US-A- 5 680 863, Fig. 4 and 6 as well as the corresponding description. These claims in combination with any of Claims 45, 47 and/or 49 could not serve as a basis for an independent that would novel and inventive.

The additional features described in Claim 51-53 and 55-56 do not involve an inventive step since they do not produce any unexpected effect. The inclusion of these features in an acoustic array is a current practice for the skilled person.

None of the cited documents appears to anticipate or suggest the collection of features as defined by the combination of Claims 45 and 54. This claim meets therefore the requirements of Art. 33(2), 33(3) PCT.

The subject-matter of Claims 66 and 67 is not inventive since the device resulting in applying the manufacturing method is known and that the individual method steps and/or their succession are the steps that the skilled person would a priori undertake to manufacture such a device. None for these steps or the succession of the latter appear to generate an unexpected effect.

The subject-matter of Claims 68 and 69 is not inventive since the bare fact of using a pleated or undulated transmission-line-to-electrically-interconnect two electrical devices so as to provide mechanical damping there along is a common place, in particular when one of the device is physically , irrespectively of the type of electrical

devices interconnected. And obviously, applying this technique to a transducer array does not produce any surprising effect, whatever the type of transducer array or sensor elements.

3. Claims 57-65, 70-73

Claim 70 : None of the documents cited in the International Search Report discloses a method of arranging an acoustic sensor array onto a patient with features as recited in Claim 70. None of the documents cited against Claims 70 discloses or suggests to peel off the carrier from the acoustic sensor elements once the latter have been attached to the patient. Claim 70 meets therefore the requirements of Art. 33(2), 33(3) PCT.

Claims 71-73 : These claims contain miscellaneous features of particular embodiments of the method claimed in Claim 70. They also meet the requirements of Art. 33 (2), 33(3) PCT.

Re Item VII

Certain defects in the international application

0. Remarks applying to all groups of claims :

0.1 Reference signs in parentheses should be inserted in the claims to increase their intelligibility (Rule 6.2(b) PCT). This applies to both the preamble and characterising portion of all claims, independent or dependent.

0.2 In the citations of prior art document at several places in the description, see e.g. pg. 1, 2, 18, 20, 23 or 30, the formulation "the specification thereof being specifically incorporated herein by reference" is contrary to the PCT Guide Lines II, 4.17. These formulations should be deleted from the description.

~~0.3~~ In the citations of prior art patent documents at several places in the description, see e.g. pg. 1 and 2, publication numbers should be cited instead of application numbers.

- 0.4 The respective parts of description must be brought into conformity with the new claims to be filed. Care should be taken during revision, especially of the introductory portion including any statements of problem or advantage, not to add subject-matter which extends beyond the content of the application as originally filed, Article 34(2)(b) PCT.

In order to avoid further objections concerning Article 34(2)(b) PCT and to expedite the procedure, detailed indications concerning the locations where the features of each new claim had originally been disclosed should be supplied.

- 0.5 The numerical values expressed in micron units at various places in the description and in the claims do not meet the requirements of Rule 10.1(a) PCT and should be replaced by the appropriate values in SI units. The present expressions should, however, be retained in parentheses after the replacement expressions.
- 0.6 The general statement in the description at page 43, last line is not clear, and when used to interpret the claims renders them also unclear, contrary to Article 6 PCT. This statement should therefore be deleted.

1. Claims 1-44

- 1.1 To meet the requirements of Rule 6.3(b) PCT, the independent apparatus claims should be properly cast in the two part form, with all those features which in combination are part of the prior art (see respectively document D11 for the sensor element and D12 for the sensor array) being placed in the preamble.
- 1.2 Documents D11 and D12 should be referred to in the description as representing the nearest prior art for respectively the sensor element and the sensor array and the relevant background art disclosed therein is to be indicated (Rule 5.1(a)(ii) PCT).

2. Claims 45-56, 66-67, 68-69

- 2.1 To meet the requirements of Rule 6.3(b) PCT, the independent apparatus claim should be properly cast in the two part form, with all those features which in combination are part of the prior art (see document D21) being placed in the preamble.
- 2.2 Document D21 should be referred to in the description as representing the nearest prior art and the relevant background art disclosed therein is to be indicated (Rule 5.1(a)(ii) PCT).

3. Claims 57-65, 70-73

Nihil.

Re Item VIII

Certain observations on the international application

1. Claims 1-44

- 1.1 As a general remark, the applicant's attention is drawn to the fact that the requirement of Article 6 PCT that the claims shall be concise does not only refer to the individual claims but also to the claims in their entirety. Undue repetition of wordings has to be avoided by the use of the dependent form.

The presence of a multiplicity of independent claims of overlapping subject-matter renders obscure (Art. 6 PCT) the matter for which protection is sought, in particular as far as the sensor array is concerned.

Moreover, if the present application relates to one invention only, as set out in Rule 13.1 PCT, it must be possible to group the independent claims in such a way that no superfluous repetitions are necessary. The arrangement must therefore be one which enables the association of related claims to be readily determined and their meaning in association to be readily construed.

In the present application there would seem to be no reason why a first

independent claim for the acoustic sensor element (described in terms of detailed structural details) and a subsequent claim for an acoustic sensor array explicitly referring to the independent claim claiming the acoustic sensor element would not suffice.

- 1.2 Claim 1 is unclear since it does not define the sensor elements in terms of structural features.

Indeed the formulation "sensor element configured so as to ..." is a functional formulation, i.e. indicating the result to be obtained without providing the structural features defining the means necessary for achieving the desired result. Such a formulation is not allowable since the person skilled in the art would have to employ an inventive step in order to find a solution to the problem posed.

Since this feature is in fact the nucleus of the claimed invention by which it is distinguished over the prior art, it has to be incorporated into Claim 1 and described in terms of structural details allowing to readily understand the solution to the stated problem (Art.6 taken in combination with Rules 6.3 (a) and (b) PCT).

The expression "frequency range of interest" is totally obscure and does not allow at all to infer which structural features are necessary to solve the stated problem.

Moreover, the term "compressional wavelengths" is totally obscure and does not appear to designate any well known physical entity.

- 1.3 In Claim 2, the wording "sensor frame" is misleading since it seems to imply that the frame is part of the sensor. However, it seems that the frame only acts as a support for the sensor elements.

- 1.4 In Claim 2, the expression "each of said sensor elements has a pliable configuration" is unclear since no well defined structural features can be derived from it : a "pliable configuration" could be understood as the elements being made of flexible resilient material or as the elements being made of flexible non-resilient material or ... or as the elements being arranged in a series of articulated rigid elements (such as in a chain). At least the two latter embodiments are, however, not supported by the description.

- 1.6 Claim 6 makes an unallowable reference to an item (the subject on which the sensor elements are applied) which is not part of the apparatus to be protected.

Such formulation should be avoided. The claimed apparatus must be described with detailed structural features which clearly and unambiguously define it per se.

- 1.7 In Claim 18, the use of the wording "pliable" does not imply that the corresponding parts of the sensor elements are actually flexible (in the sense that they will regain their original shape after deformation). As already stated under Section VIII.1.4, this formulation includes embodiments which are not supported by the description.
- 1.8 In Claim 18, it is unclear how the two voltage signals could have an opposed polarity if there is no common reference voltage plane. However, such a reference voltage plane does not appear to be defined in Claim 18.
- 1.9 It seems that an inversion occurred in Claim 23, see pg. 19, l. 5-7. The actual wording is not supported by the description.
- 1.10 The objections detailed in Sections VIII.1.3 and VIII.1.4 apply also to Claim 26.
- 1.11 The features of Claim 28 and 29 are only described in functional terms, therefore a corresponding objection as explained in VIII.1.2 applies to these claims as well.
- 1.12 It follows from the requirements of Art.6 taken in combination with Rules 6.3 (a) and (b) PCT that any independent claim should include all the features necessary to solve the stated problem.

This is not the case when reading independent Claims 1, 18, 26, 37 and 44.

It will be noted, e.g. that applying the method of Claim 37, results in a array having sensor elements with well-defined structural features whilst no such features are present in Claim 1.

These inconsistencies could be removed by adopting the solution proposed in Section VIII.1.1.

2. Claims 45-56, 66-67, 68-69

2.1 Claim 46 is totally obscure.

2.2 In Claims 53, the nature of the reflective surface should be specified, i.e. acoustically or optically or else. Its location should be specified as well, i.e. on the first or second surface.

2.3 Claim 55 (which depends on claim 45 via Claim 54) appears to repeat a feature of Claim 45 and is therefore not concise. This claim should be dropped.

2.4 It appears that the feature of Claim 67 should be included in Claim 66.

Indeed, it appears from the wording of independent Claim 45 that each transmission is configured with a series of undulations along its lengths. However, Claim 66 does not include a corresponding feature. The method of Claim 66 would therefore not result in an acoustic array as claimed in Claim 45, contrary to the statement at the second line of Claim 66.

Moreover, since independent Claim 66 does not contain this feature, it does not meet the requirement following from Article 6 taken in combination with Rules 6.3 (a) and (b) PCT that any independent claim must contain all the technical features essential to the invention.

3. Claims 57-65, 70-73

3.1 Claim 57 is totally unclear.

Claim 57 appears to define an acoustic sensor array of sensors having no one well defined structural feature with the exception of having two outer surfaces.

Even this latter feature is not clear since it is not specified how these surfaces are located with respect to one another and whether they are major surfaces or not.

Moreover, the fact that one of the outer surface is configured to attach to a subject such that it is substantially conformal to the subject is absolutely not clear. Not only does this definition makes an unallowed reference to an item which is not part of the array (i.e. the subject to inspect), but moreover this "subject" has a priori no well defined features or properties. The technical structural features that make the sensor elements compliant and allow them to attach to anything should therefore be defined.

The features defining the carrier member are also unclear since they attempt to defined the carrier member only in terms of functional features, i.e. indicating the result to be obtained without providing the structural features defining the means necessary for achieving the desired result. Such formulations are not allowable since the person skilled in the art would have to employ an inventive step in order to find a solution to the problem posed.

Therefore the carrier member should be defined with structural details and corresponding structural details of the sensor surfaces allowing to understand how it is realisable attached to the sensor elements, how it forces said elements into alignment and how it can be disengaged from them without causing the sensor elements to move.

From the preceding, it is also fully unclear where the electrodes of the sensor elements could possibly be located.

- 3.2 In Claims **60**, **62** and **73**, the nature of the reflective surface should be specified, i.e. acoustically or optically or else. Its location should be specified as well, i.e. on the first or second surface.
- 3.3 Claim **61** is in contradiction with Claim 57 which states that the sensor elements are compliant so as to be conformal to the subject to inspect. However, if according to Claim 61, stiffener are attached to said sensor elements, the latter would not be compliant any more.
-
- 3.4 Claim **70** should specify by which means the sensor elements are hold on the unitized carrier so as to allow the latter to be peeled off the former. Some

**INTERNATIONAL PRELIMINARY
EXAMINATION REPORT - SEPARATE SHEET**

International application No. PCT/US00/05124

properties of the carrier member should also be specified so as to explain how the carrier member can be conformed to the patient attaching surface. Indeed, were the carrier rigid, the various sensor elements could not a priori be attached to the patient. Moreover, such an embodiment is not supported by the description.

INTERNATIONAL SEARCH REPORT

(PCT Article 18 and Rules 43 and 44)

Applicant's or agent's file reference 9023.21.W0	FOR FURTHER ACTION see Notification of Transmittal of International Search Report (Form PCT/ISA/220) as well as, where applicable, item 5 below.	
International application No. PCT/US 00/ 05124	International filing date (day/month/year) 29/02/2000	(Earliest) Priority Date (day/month/year) 01/03/1999
Applicant MEDACOUSTICS, INC. et al.		

This International Search Report has been prepared by this International Searching Authority and is transmitted to the applicant according to Article 18. A copy is being transmitted to the International Bureau:

This International Search Report consists of a total of 5 sheets.



It is also accompanied by a copy of each prior art document cited in this report.

1. Basis of the report

- a. With regard to the **language**, the international search was carried out on the basis of the international application in the language in which it was filed, unless otherwise indicated under this item.



the international search was carried out on the basis of a translation of the international application furnished to this Authority (Rule 23.1(b)).

- b. With regard to any **nucleotide and/or amino acid sequence** disclosed in the international application, the international search was carried out on the basis of the sequence listing :



contained in the international application in written form.



filed together with the international application in computer readable form.



furnished subsequently to this Authority in written form.



furnished subsequently to this Authority in computer readable form.



the statement that the subsequently furnished written sequence listing does not go beyond the disclosure in the international application as filed has been furnished.



the statement that the information recorded in computer readable form is identical to the written sequence listing has been furnished

2. ☐ Certain claims were found unsearchable (See Box I).

3. ☒ Unity of invention is lacking (see Box II).

4. With regard to the title,



the text is approved as submitted by the applicant.



the text has been established by this Authority to read as follows:

LOW PROFILE ACOUSTIC SENSOR ARRAY AND SENSORS WITH PLEATED TRANSMISSION LINES AND RELATED METHODS

5. With regard to the abstract,



the text is approved as submitted by the applicant.



the text has been established, according to Rule 38.2(b), by this Authority as it appears in Box III. The applicant may, within one month from the date of mailing of this international search report, submit comments to this Authority.

6. The figure of the drawings to be published with the abstract is Figure No.



as suggested by the applicant.



because the applicant failed to suggest a figure.



because this figure better characterizes the invention.

1b



None of the figures.

INTERNATIONAL SEARCH REPORT

International Application No

T/US 00/05124

A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 B06B1/06 A61B7/04

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7 B06B A61B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO 98 22786 A (FLOWSCAN INC) 28 May 1998 (1998-05-28)	18-25
Y	page 1, line 1 - line 18 page 4, line 28 -page 7, line 28 page 11, line 37 -page 12, line 9 ---	1,44
Y	US 5 807 271 A (SOULUER FARID ET AL) 15 September 1998 (1998-09-15) column 1, line 5 - line 7 column 3, line 49 - line 58; claim 1; figure 3 ---	1,44
A	EP 0 420 190 A (ATOCHEM NORTH AMERICA) 3 April 1991 (1991-04-03) page 2, column 1, line 10 - line 15 page 4, column 5, line 45 -page 5, column 7, line 21 page 6, column 9, line 20 - line 45 --- -/--	1,18,37

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

° Special categories of cited documents :

- *A* document defining the general state of the art which is not considered to be of particular relevance
- *E* earlier document but published on or after the international filing date
- *L* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- *O* document referring to an oral disclosure, use, exhibition or other means
- *P* document published prior to the international filing date but later than the priority date claimed

- *T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- *X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- *Y* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- * & * document member of the same patent family

Date of the actual completion of the international search

27 September 2000

Date of mailing of the international search report

19.10.00

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
Fax: (+31-70) 340-3016

Authorized officer

Lorne, B

INTERNATIONAL SEARCH REPORT

International Application No

T/US 00/05124

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4 833 659 A (GEIL FREDERICK G ET AL) 23 May 1989 (1989-05-23) column 3, line 47 -column 4, line 23 column 6, line 37 -column 7, line 57 ---	1
A	WO 94 30030 A (UNIV CALIFORNIA) 22 December 1994 (1994-12-22) page 5, line 7 -page 8, line 24 ---	26
X	US 5 795 299 A (BRUMMER CHARLES W ET AL) 18 August 1998 (1998-08-18) column 1, line 49 -column 2, line 3 column 2, line 55 -column 3, line 13 column 4, line 16 - line 41; claim 1 ---	45-47,49
A	US 5 398 689 A (CONNOR BRIAN G ET AL) 21 March 1995 (1995-03-21) column 1, line 40 -column 2, line 26; claim 1 ---	66,68
A	US 5 680 863 A (COOPER THOMAS G ET AL) 28 October 1997 (1997-10-28) column 1, line 46 -column 2, line 31 ---	45
A	EP 0 801 927 A (MEDACOUSTICS INC) 22 October 1997 (1997-10-22) page 3, column 3, line 48 -column 4, line 24; claims 1,2 ---	57,70
A	US 5 598 845 A (STERN ROGER A ET AL) 4 February 1997 (1997-02-04) column 2, line 65 -column 3, line 8 column 4, line 1 - line 35; figures 2,3 ---	57,70
A	US 4 308 870 A (ARKANS EDWARD J) 5 January 1982 (1982-01-05) the whole document -----	57,70

Box I Observations where certain claims were found unsearchable (Continuation of item 1 of first sheet)

This International Search Report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. ☐ Claims Nos.:
because they relate to subject matter not required to be searched by this Authority, namely:

2. ☐ Claims Nos.:
because they relate to parts of the International Application that do not comply with the prescribed requirements to such an extent that no meaningful International Search can be carried out, specifically:

3. ☐ Claims Nos.:
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

Box II Observations where unity of invention is lacking (Continuation of item 2 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

see additional sheet

1. ☒ As all required additional search fees were timely paid by the applicant, this International Search Report covers all searchable claims.
2. ☐ As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.
3. ☐ As only some of the required additional search fees were timely paid by the applicant, this International Search Report covers only those claims for which fees were paid, specifically claims Nos.:
4. ☐ No required additional search fees were timely paid by the applicant. Consequently, this International Search Report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest.
- ☒ No protest accompanied the payment of additional search fees.

Box III TEXT OF THE ABSTRACT (Continuation of item 5 of the first sheet)

A low profile acoustic array (10) is configured to selectively respond to shear waves while rejecting compression wave energy in the frequency range of interest. One sensor array is configured as a linear strip with a frame segment having at least one longitudinally extending rail and a plurality of sensor elements (20) extending therefrom. These sensor elements have a resilient core and opposing PDVF outer layers configured with opposing polarities onto the core. The linear strip array also includes a pair of separate electrical signal transmission paths. The transmission lines can include a series of undulations formed thereon to help minimize undesired mechanical crossover between sensors. A carrier member can be configured to be detachably releasable carries the discrete sensors to maintain the positional alignment until they are secured to a patient.

FURTHER INFORMATION CONTINUED FROM PCT/ISA/ 210

This International Searching Authority found multiple (groups of) inventions in this international application, as follows:

1. Claims: 1-44

A low profile acoustic sensor array comprising strips with sensor elements mounted on frames with rails.

2. Claims: 45-56, 66-67, 68-69

Configuration of transmission lines with a series of undulations in the transmission paths.

3. Claims: 57-65, 70-73

A carrier member to hold the plurality of sensors.

INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/US 00/05124

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
WO 9822786	A	28-05-1998	US 5827198 A AU 4750397 A	27-10-1998 10-06-1998
US 5807271	A	15-09-1998	NONE	
EP 0420190	A	03-04-1991	US 5166573 A CA 2026053 A JP 3207200 A	24-11-1992 27-03-1991 10-09-1991
US 4833659	A	23-05-1989	NONE	
WO 9430030	A	22-12-1994	AU 6953994 A US 5633552 A US 5569968 A US 5728089 A	03-01-1995 27-05-1997 29-10-1996 17-03-1998
US 5795299	A	18-08-1998	NONE	
US 5398689	A	21-03-1995	DE 9402697 U JP 7008494 A	14-04-1994 13-01-1995
US 5680863	A	28-10-1997	US 5735282 A	07-04-1998
EP 0801927	A	22-10-1997	US 5365937 A AU 5099693 A CA 2144169 A DE 69323085 D DE 69323085 T EP 0659058 A WO 9405207 A US 5807268 A US 5913829 A	22-11-1994 29-03-1994 17-03-1994 25-02-1999 24-06-1999 28-06-1995 17-03-1994 15-09-1998 22-06-1999
US 5598845	A	04-02-1997	AU 717213 B AU 7599996 A CA 2237967 A EP 0862381 A WO 9717883 A	23-03-2000 05-06-1997 22-05-1997 09-09-1998 22-05-1997
US 4308870	A	05-01-1982	CA 1166701 A	01-05-1984

FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AL	Albania	ES	Spain	LS	Lesotho	SI	Slovenia
AM	Armenia	FI	Finland	LT	Lithuania	SK	Slovakia
AT	Austria	FR	France	LU	Luxembourg	SN	Senegal
AU	Australia	GA	Gabon	LV	Latvia	SZ	Swaziland
AZ	Azerbaijan	GB	United Kingdom	MC	Monaco	TD	Chad
BA	Bosnia and Herzegovina	GE	Georgia	MD	Republic of Moldova	TG	Togo
BB	Barbados	GH	Ghana	MG	Madagascar	TJ	Tajikistan
BE	Belgium	GN	Guinea	MK	The former Yugoslav Republic of Macedonia	TM	Turkmenistan
BF	Burkina Faso	GR	Greece			TR	Turkey
BG	Bulgaria	HU	Hungary	ML	Mali	TT	Trinidad and Tobago
BJ	Benin	IE	Ireland	MN	Mongolia	UA	Ukraine
BR	Brazil	IL	Israel	MR	Mauritania	UG	Uganda
BY	Belarus	IS	Iceland	MW	Malawi	US	United States of America
CA	Canada	IT	Italy	MX	Mexico	UZ	Uzbekistan
CF	Central African Republic	JP	Japan	NE	Niger	VN	Viet Nam
CG	Congo	KE	Kenya	NL	Netherlands	YU	Yugoslavia
CH	Switzerland	KG	Kyrgyzstan	NO	Norway	ZW	Zimbabwe
CI	Côte d'Ivoire	KP	Democratic People's Republic of Korea	NZ	New Zealand		
CM	Cameroon			PL	Poland		
CN	China	KR	Republic of Korea	PT	Portugal		
CU	Cuba	KZ	Kazakstan	RO	Romania		
CZ	Czech Republic	LC	Saint Lucia	RU	Russian Federation		
DE	Germany	LI	Liechtenstein	SD	Sudan		
DK	Denmark	LK	Sri Lanka	SE	Sweden		
EE	Estonia	LR	Liberia	SG	Singapore		



DK (utility model), EE, EE (utility model), ES, FI, FI (utility model), GB, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SK (utility model), SL, TJ, TM, TR, TT, UA, UG, US, UZ, VN, YU, ZA, ZW.

- (84) **Designated States (regional):** ARIPO patent (GH, GM, KE, LS, MW, SD, SL, SZ, TZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG).

Published:

— with international search report

- (88) **Date of publication of the international search report:**
26 July 2001

- (48) **Date of publication of this corrected version:**
25 October 2001

(15) Information about Correction:

see PCT Gazette No. 43/2001 of 25 October 2001, Section II

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

**LOW PROFILE ACOUSTIC SENSOR ARRAY AND
SENSORS WITH PLEATED TRANSMISSION LINES
AND RELATED METHODS**

Field of the Invention

The present invention relates generally to disposable acoustic sensors for capturing sounds from within the human body. The acoustic sensors are particularly useful for non-invasive digital acoustic cardiography, phonography, and acoustic spectral analysis applications.

Background of the Invention

Recently, acoustic sensors have been used for the non-invasive detection of coronary artery disease. See co-assigned and co-pending U.S. Patent Application Serial No. 09/188,510 entitled "*Non-Invasive Turbulent Blood Flow Imaging System*," the contents of which are hereby incorporated by reference as if recited in full herein. Generally stated, in operation, sensors are configured on a patient's chest (*i.e.*, contacting the external epidermal surface or skin) to generate an electrical signal in response to a detected acoustic wave. The detected acoustic wave signals are processed to identify features that indicate the condition of a patient's coronary arteries, specifically the presence or absence of lesions that limit the flow of blood through the coronaries. An essentially uniform display indicates normal blood flow, while a non-uniform display may indicate abnormal (turbulent) blood flow and/or the presence of an occlusion.

In the above-described non-invasive systems, the acoustic sensors are positioned over the chest cavity in an acoustic window as described in co-pending and co-assigned U.S. Patent Application Serial No. 09/188,434 entitled, "*Acoustic Sensor Array For Non-Invasive Detection of Coronary Artery Heart Disease*," the

contents of which are hereby incorporated by reference as if recited in full herein.

In position, the sensors are preferably configured over the intercostal space so as to reliably generate data signals corresponding to the blood flow of the patient during

each phase of the cardiac cycle. The acoustic sensor is preferably designed to

5 sense the flexing of a patient's external epidermal surface (skin) that is a result of the localized nature of the internal heart sounds. The sensor is also preferably easy to position on a patient and inexpensive such that it can be a single use device,

which is disposable after use. In operation, the sensor is preferably configured to

be conformal to the chest configuration of a patient (which varies patient to patient)

10 and is also preferably configured to generate the electrical signal based on the flexure of the skin. Unfortunately, poor correlation of signals from improper

sensor positioning, array geometry, and/or sensor configurations can adversely affect the reliability and/or correlation of the detected acoustic signal. Indeed, one

potentially problematic sensor characteristic is that it can generate signals which

15 are not representative of the interested acoustic wave associated with the blood flow of a patient, *i.e.*, it can be responsive to extraneous acoustic waves and noise.

Conventional acoustic sensors can have poor signal to noise ratio (SNR) in that they can be unduly sensitive to environmental noise (typically requiring a

special, quiet room be used for acoustic applications) or can suffer from low

20 sensitivity relative to its electrical floor. Other sensors have other performance

deficiencies such as inadequate sensitivity. In addition, many sensors are relatively complex configurations which can make them expensive to produce and difficult to apply clinically.

An example of a conventional disposable acoustic pad sensor is illustrated

25 in U.S. Patent Application Serial No. 08/802,593. The sensor includes a plurality of layers of various materials connected at one end to a substantially rigid

electrostatic shield and electrical connector. Another example of an acoustic

sensor is shown in U.S. Patent Application Serial No. 09/136,933. This sensor is a flexible thin-film sensor which includes a foot portion and a two-piece

30 piezoelectric film support. Still other examples of acoustic sensors are described in U.S. Patents 5,365,937, and 5,807,268. These sensors employ an air gap and a

frame which acts to stretch and hold a polymer film in tension. However, there remains a need to provide improved sensors for the efficient and improved passive detection of heart and blood-flow acoustics.

5

Objects and Summary of the Invention

It is therefore an object of the present invention to provide an improved low profile sensor which is configured to be substantially conformal to a patient's external epidermal surface.

10

It is an additional object of the present invention to provide an improved sensor which provides a high signal to noise ratio for the acoustic energy of interest.

15

It is another object of the invention to provide an improved disposable sensor array with a plurality of individual sensor elements which are conformal to the underlying epidermal surface when positioned on a patient and which are proximately positioned one sensor to the next in a manner which allows an increased number of sensor elements within an acoustic region of interest and which positions the individual sensor elements such that they are separately responsive to preferred acoustic wave lengths.

20

It is an additional object of the invention to provide a sensor array which reduces the potential for undesired signal crossover along the separate electrical paths for the sensor elements.

25

It is yet another object of the invention to provide a transmission path for each of the individual sensors in a sensor array in a manner which reduces mechanical and electrical crossover between the sensors and/or external mechanical input into the sensor signal path.

30

It is another object of the invention to provide an improved method and device to install and align discrete sensor elements onto a subject.

These and other objects of the present invention are provided by a low profile acoustic sensory array which acts as a mechanical filter to minimize the sensor's signal activation or response to extraneous and/or undesired acoustic wavelengths or non-relevant acoustic wave components. Such a device is

selectively responsive to short wavelengths that cause flexure through the thickness of the sensor, while resistant to longer acoustic wavelengths. The longer wavelengths are typically associated with compression waves in the body or in ambient noise within the examining room, and which can cause compression through the thickness of the sensor. In operation, due to the differences in the speed of the waves over a frequency band, shear waves typically have much shorter wavelengths than the wavelengths associated with compression waves. Stated differently, the sensor of the present invention is responsive to the flexural mode of displacement created by short wavelengths of shear waves, and substantially non-responsive to acoustic inputs of the much longer compression wavelengths.

Thus, one embodiment of the present invention provides a low profile flexural responsive sensor array which is sized and configured to substantially reject compression energy while responding to shear energy in the frequency range of interest. The sensor array includes a plurality of proximately positioned sensor elements. Preferably the sensor elements include two active surfaces, each of which lies on opposite sides of a neutral layer, such that the sum of the two layers produces a signal responsive to the flexure or change in curvature of the underlying surface since, in operation, they are displaced from the neutral axis of the structure

More particularly, a first aspect of the invention is directed toward a low profile acoustic sensor array. The array includes a plurality of longitudinally extending sensor strips. Each of the sensor strips comprises a sensor frame having at least one longitudinally extending rail having a length. The sensor strips also include a plurality of acoustic sensor elements attached to the at least one rail. The sensor element has a pliable configuration. The strips also include a plurality of separate electrical signal paths, at least one (and in a preferred embodiment, two spatially separate and opposing paths) for each of the sensor elements. The electrical signal paths define a signal path from a respective one of each of the sensor elements to a desired end electrical termination point.

Preferably, the sensor array signal path is configured such that each sensor element includes first and second PVDF film layers and an intermediate neutral core, each PVDF film layer has an associated internal PVDF film surface (defining

the live signal paths and electrodes), and corresponding first and second external ground surfaces (forming the ground plane).

In a preferred embodiment, the frame is configured with first and second transversely opposing sides. The opposing sides of the frame are spatially separated along a major portion of the frame length and each of the sensor elements is attached to a selected one of the frame sides. In this embodiment, the acoustic sensor element is sized and configured to extend between the sensor frame opposing sides. It is also preferred that the sensor elements are arranged on the frame such that adjacent elements are attached to different sides of the frame. Preferably, each of the strips is a unitary body along a major portion of its length, and the sensor elements are linearly aligned along the strip.

Another aspect of the present invention is directed toward an individual acoustic sensor element. The acoustic sensor element comprises a resilient core layer, preferably comprising a low permittivity material, having a core thickness and a first pliable material layer overlaying and contacting the core layer. The first pliable material layer comprises a piezoelectrically active material and has opposing internal and external surfaces. The sensor element also includes a second pliable material layer overlaying and contacting the core layer opposite the first pliable material layer. The second pliable layer comprises a piezoelectrically active material and also has opposing internal and external surfaces. The first material layer includes a first electrical trace disposed on the internal surface and the second material layer includes a second electrical trace disposed on its internal surface. During operation, and in response to flexure of said sensor element, the first and second electrical traces generate respective first and second voltages and the first and second voltages have opposing polarity.

In a preferred embodiment, the core comprises neoprene and the first and second pliable layers are formed from PVDF. Also preferably, the core layer has a first relative permittivity and the first and second pliable material layers have a second relative permittivity. The first relative permittivity is less than the second relative permittivity. As such, the resulting capacitance of the core may be such that it is about an order of magnitude less than the PVDF. In a preferred

embodiment, the core is sized to have a greater thickness than the PVDF layers. Capacitance is related to the permittivity (ϵ), the area (A) and the thickness (l), as stated by the equation ($C=\epsilon A/l$); therefore, the core is preferably configured to have a capacitance which is less than that of the PVDF layers. As such, the sensor configuration will be such that the two permittivities typically differ by about a factor of two (because the core is configured to be thicker than the PVDF).

An additional aspect of the present invention is similar to the multiple strip array but is directed toward a single acoustic strip sensor array, the single strip array comprises a sensor frame having a frame length with at least one longitudinally extending rail. The strip also includes a plurality of sensor elements attached to the rail. The sensor element has a pliable configuration. The strip also includes opposing spatially separate first and second electrical signal paths for each of the sensor elements. The first and second electrical signal paths define a first and second signal transmission path from a respective one of each of the sensor elements to a desired end electrical termination point. Preferably, the acoustic strip sensor defines a substantially planar profile along at least the frame when viewed from the side. In a preferred embodiment, the frame and sensor elements are sized and configured (during operation and in position on a patient) to flex in response to flexural movement associated with shear waves while undergoing gross translation in response to long compressional waves (thus inhibiting sensor response associated with the long compressional waves). Preferably, the size of the acoustic strip sensor elements are such as to allow intercostal placement on the subject. In particular, each sensor element is sized and configured with dimensions of from about 8 mm to about 11 mm in length and width may be suitable, however, other sizes may also be utilized. It is also preferred that the first and second electrical signal paths are positioned to face each other on opposing sides of the core. In an alternative preferred embodiment, a discrete mass or stiffener is positioned to overlay each of the sensor elements.

Another aspect of the present invention is directed toward an acoustic coronary artery detection method employing the differential signal output associated with a flexed sensor as described above.

Yet another aspect of the present invention is directed toward a method for fabricating a strip sensor. The method includes the steps of forming a unitary body strip sensor foundation layer and forming a series of proximately positioned non-contacting pads and a frame segment into the foundation layer. Two separate
5 opposing PVDF layers are positioned on opposing major surfaces of the foundation layer. The PVDF layers include two major surfaces and an electrical signal path formed on one surface and a ground path formed on the other. The method also includes the step of orienting the PVDF layers such that the electrical signal paths of each of the PVDF layers faces the foundation layer. Preferably, a series of
10 corresponding but electrically separate external traces are disposed onto the major surfaces of the PVDF layers.

Preferably, the PVDF layers are selectively "actively" polarized about the sensor pad regions and substantially non-activated about the longitudinally extending sides or rails. Optionally, predetermined portions of the longitudinally
15 extending sides can be heated to depolarize selective areas of the longitudinally extending sides or rails. In a preferred embodiment, a conductive outer ground plane is formed over the PVDF material such as by depositing a conductive material layer or forming metallized mylar over the top and bottom of the PVDF material surfaces (the surfaces facing away from the core).

20 An additional aspect of the present invention is directed to an accordion-pleated discrete or unitized element sensor array. More particularly, this aspect is directed to an acoustic sensor array which comprises a plurality of unitary acoustic sensor elements and a plurality of transmission lines having opposing first and second ends and defining a length therebetween, a respective one transmission line
25 for each of the plurality of unitary acoustic sensors. The first end of the transmission line is individually attached to one of the acoustic sensor elements. Each of the transmission lines is configured with a series of undulations along its length. In a preferred embodiment, the undulations are a series of continuous pleated segments.

30 Another embodiment of the present invention is directed to an acoustic sensor. The acoustic sensor comprises a sensor element and a transmission line.

The sensor element comprises a resilient core layer comprising a low permittivity material having a core thickness and a first pliable material layer sized and configured to sandwich and overlay the core layer. The first material layer comprises a piezoelectrically active material having opposing first and second major surfaces. First and second electrical traces are disposed on the first major surface of the first pliable material layer. The first pliable layer and associated electrical traces define a respective first and second electrode such that when in position over the core, the first electrode has an opposite polarity relative to the second electrode. Preferably, the sensor element also includes an exterior
5
10
15
20
25
30
conductive shield layer sized and configured to overlay the second major surface of the first material layer.

The sensor additionally includes a linear transmission line attached to the sensor element. The linear transmission line includes first and second ends and longitudinally extends therebetween. The transmission line comprises a first pliable material layer extending from the first end to the second end of the linear transmission line. The first pliable layer has opposing first and second major surfaces and comprises a piezoelectrically active material. The transmission line also includes first, second, and third electrical traces disposed on the first pliable material layer in electrical communication with the sensor element first material layer electrical traces. The first and second electrical traces are disposed on the first major surface and the third electrical trace is disposed on the second major surface. The transmission line also includes first and second layers of a non-conducting film configured and sized to overlay a major portion of the first and second major surfaces of the first pliable material layer. The transmission line additionally includes a first linear outer layer conductive strip configured and sized to overlay a major portion of the first non-conducting film layer opposing the first major surface of the first pliable material layer and a second linear outer layer conductive strip configured and sized to overlay a major portion of the second non-conducting film layer opposing the second major surface of the first pliable material layer. The first pliable material layer of the transmission line and the sensor element is a unitary layer and the third electrical trace of the first pliable
15
20
25
30

material layer provides an electrical ground operably associated with the first and second conductive outer layers of the sensor. In a preferred embodiment, the acoustic sensor transmission line is configured with a series of undulations along its length.

5 Yet another aspect of the present invention is an acoustic sensor array, comprising a plurality of sensor elements having first and second outer surfaces. The first outer surface is configured to attach to a subject. The sensor array also includes a carrier member release-ably attached to the second outer surface of each of the plurality of sensor elements to hold the plurality of sensors in alignment. In
10 operation, the carrier member is disengaged from the sensor elements after the sensor elements are attached to the subject. In one embodiment, the sensor elements are a set of discrete (structurally separate) sensor elements and the carrier member maintains positional alignment of the sensor elements for easier positioning onto a subject. Advantageously, the carrier member can also be used
15 for other sensor configurations, and is particularly useful for resilient or compact flexural element configurations (such as the strip sensor embodiment described herein).

An additional aspect of the present invention is directed to a method of minimizing the mechanical interference between one or more of adjacent sensors
20 and the end of the transmission line. For example, the method can minimize interference between adjacent sensors and system or environment mechanical forces which potentially can be input to the sensor by mechanically isolating flexure responsive acoustic sensor elements in arrays having a plurality of sensor elements. The method comprises the step of forming a series of undulations in a
25 electrical transmission path to provide mechanical damping therealong. Preferably, the acoustic sensor array includes a plurality of sensor elements and a separate electrical transmission path for each of said sensor elements and the method further comprises the step of forming the sensor array such that the plurality of sensor elements and associated sensor electrical transmission paths are physically separate
30 units.

Another aspect of the present invention is a method of forming an acoustic

sensor having a sensor pad region and a transmission line, comprising the steps of configuring a first unitary layer of PVDF film having first and second opposing major surfaces with a laterally extending region having a first width and a longitudinally extending region having a second width. Electrical traces are formed onto the first major surfaces of the PVDF layer. The sensor electrical traces are arranged as rectangular shapes onto the lateral region of the PVDF layer such that the lateral region defines first and second separate electrode regions with opposing polarity. Electrical traces are formed onto the longitudinally extending region of the first and second major surfaces of the PVDF layer to define three electrical paths. The first and second paths are formed on one major surface to provide the electrical signal path for the first and second electrode regions, and the third path is formed on the opposing major surface of the PVDF layer and is configured with a primary finger portion. A resilient core is inserted onto a surface of one of the electrode regions and non-conducting film is positioned to overlay substantially the entire length of both major surfaces of the longitudinally extending region of the PVDF layer. A first electric shield material is positioned to overlay the non-conducting film on the side opposing the first major surface of the PVDF film. The first electrical shield includes a conductive secondary finger portion. A second electric shield layer is provided. The second shield layer is configured and sized to mirror the PVDF film shape and is positioned to overlay the second major surface of the PVDF film in the laterally extending electrode region and to overlay and contact the non-conducting film in the longitudinally extending region. The laterally extending region of the PVDF film is folded over the core such that the first and second electrode regions are positioned opposing the other with the core is positioned intermediate thereof. The primary finger of the ground strip is folded over to provide a terminal connection for the ground. The shield material thereby provides a substantially continuous electric shield for the externally exposed sensor body. Preferably, the method also comprises the step of forming undulations along a portion of the length of the longitudinally extending region.

Each of the sensors or sensor array embodiments of the present invention

may also include one or more discrete masses or stiffeners positioned in one or more regions of the of sensor element to facilitate the flexural response of the sensor. Preferably, the discrete masses or stiffeners are positioned on the external surface (away from the patient's skin) and can include a reflective surface to allow photogrammetric alignment means for the convenient operation of the detection system. In one preferred embodiment, the discrete mass is about 5 grams of high-density material and is laterally positioned to extend in a central region across the width of the sensor pad. Advantageously, this discrete mass can improve the sensitivity of the sensor element over a frequency band of interest, particularly the frequency band used in the passive analysis of coronary-generated acoustic sounds.

The present invention is advantageous because the low profile sensor array allows for a low center of gravity, is relatively easy to manufacture, and is resiliently configured to be conformal to the epidermal outer layer. In addition, the low profile sensor can act as a mechanical filter such that it is responsive to shear waves but relatively non-responsive to compressive wavelengths in the frequency range of interest.

Further, the strip array sensor of the instant invention is configured in a smaller package with a substantially constant and flat profile and is advantageously configured to allow additional sensors to be spatially positioned with separate electrical signal paths in close proximity, thereby allowing increased number of sensor elements to be positioned on a patient in the region of interest.

Alternatively, the instant invention configures a series of aligned but discrete conformal flexural sensors with correspondingly separate transmission lines which are configured to respond to shear waves while being substantially non-responsive to acoustic inputs of compression waves in the frequency range of interest (typically 100-1000 Hz). In a preferred embodiment, the transmission lines are flexible and configured with a means to substantially mechanically isolate or dampen the transmission line from the other sensors and transmission lines in the array in order to minimize any cross talk between the electrical sensor paths or to inhibit translation of undesired mechanical forces in the system operational environment. Also advantageously, a detachable carrier member can be used to

minimize the installation or site preparation time needed by an operator to position multiple sensors onto a patient.

Brief Description of the Drawings

5 **Figure 1A** is a schematic illustration of a sensor array assembly according to one embodiment of the present invention.

Figure 1B is a top view of a low profile strip sensor array according to the present invention.

10 **Figure 2** is a cross-sectional view of the low profile sensor array taken along lines 2-2 of **Figure 1B**.

Figure 3 is a cross-sectional view of the low profile sensor taken along lines 3-3 array of **Figure 1B**.

Figure 4 is side view of the sensor shown in **Figure 1B**.

15 **Figure 5** is an enlarged partial top view of an alternate embodiment of a sensor array according to the present invention.

Figure 5A is an enlarged partial top view of yet another embodiment of a sensor array according to the present invention.

20 **Figure 6** is a top view of a carrier unit or foundation structure according to a preferred embodiment of the present invention. **Figure 6** also illustrates heat applied to predetermined areas of the foundation structure to depolarize regions of the PVDF film on the frame.

Figure 7 is a top view of a silk screen or external signal trace pattern according to the present invention.

25 **Figure 8A** is an enlarged top view of a single element sensor illustrating two electrode surfaces according to an alternate embodiment of the present invention. In this figure, the signal return covering the back of the PVDF film has been removed for clarity.

Figure 8B is an enlarged top view of a sensor element shown in **Figure 1B**.

30 **Figure 9** is a schematic of a partial sectional view of the sensor element taken along lines 9-9 of **Figure 8B**.

Figure 10 illustrates a preferred array configuration positioned on the external skin or epidermal outer layer of a patient according to a preferred embodiment of the present invention.

Figure 11 illustrates a preferred array configuration with multiple strip array packages positioned in an acoustic window on a patient.

Figure 12 is a side schematic view of the sensor array shown in **Figure 11**.

Figure 13 is an electrical schematic of a sensor element according to a preferred embodiment of the present invention.

Figure 13A schematically illustrates the sensor's voltage differential signal response corresponding to strain on the sensor configured as shown in **Figure 13**.

Figures 14a-14c illustrate a preferred embodiment of a sensor's electrical response. **Figure 14a** illustrates the substantial non-response associated with a longer wavelength transmitted across the sensor situs while **Figures 14b** and **14c** show the voltage response (opposing polarity) corresponding to flexure at shorter wavelengths of interest. As shown, the voltage polarity corresponding to an upward flexure is positive for the upper PVDF layer and negative for the lower PVDF layer and the polarities reverse for a downward flexure.

Figure 14d schematically illustrates the sensor's ability to act as a mechanical filter to inhibit generating a detectable signal response for long wavelengths according to the present invention.

Figure 15 illustrates a preferred sensor array system according to the present invention.

Figure 16 and **16A** are block diagrams of preferred methods of forming a strip sensor array according to the present invention.

Figure 17A is a photographic image of a side perspective view of an alternate sensor array configuration according to the present invention, the sensor array shown in position on a subject.

Figure 17B is an enlarged photograph of the sensor array of **Figure 17A**.

Figures 18A and **18B** are photographic images of a side perspective view of the sensor array of **Figure 17A**.

Figure 19A is a top view of a preferred embodiment of a sensor film body configuration suitable for forming the sensor element for the sensor array shown in **Figure 17A**.

Figure 19B is a bottom view of the sensor film body of **Figure 19A**.

5 **Figure 20A** is an exploded diagram of a sensor body according to the present invention.

Figure 20B is a sectional view of a sensor element according to the present invention.

10 **Figure 21A** is a partial top view of a sensor film body and polyester layer according to a preferred embodiment of the present invention.

Figure 21B is a partial top view of a sensor body having multiple layers according to the present invention.

15 **Figure 22** is a top view of a sensor body according to the present invention, the view illustrating four end terminations formed by a preferred embodiment of the present invention.

Figure 23 is an enlarged photographic image of the sensor end of the sensor array of **Figure 17A** having a detachable carrier member according to the present invention.

20 **Figures 24A-E** illustrate the use of discrete masses with flexure responsive sensors according to the present invention.

Figures 25A-C show the use of external stiffeners for flexure responsive sensor elements according to the present invention. **Figure 25B** illustrates a combination of added discrete mass and stiffeners according to the present invention.

25 **Figure 26** illustrates a strip array with discrete masses according to the present invention.

Figure 27 schematically illustrates an operational shipping and application method according to the present invention.

Detailed Description of the Invention

The present invention now will be described more fully hereinafter with reference to the accompanying drawings, in which preferred embodiments of the invention are shown. This invention may, however, be embodied in many different forms and should not be construed as limited to the embodiments set forth herein; rather, these embodiments are provided so that this disclosure will be thorough and complete, and will fully convey the scope of the invention to those skilled in the art. Like numbers refer to like elements throughout. In the drawings, layers or regions may be exaggerated for clarity.

The present invention relates to a sensor array configuration and components thereof and an associated method for fabricating a sensor array. In the description of the present invention that follows, certain terms are employed to refer to the positional relationship of certain structures relative to other structures. As used herein, the term "longitudinal" and derivatives thereof refer to the general direction defined by the longitudinal axis of the sensor array that extends between the two ends of the sensor array. Thus, when positioned on a patient, the longitudinal axis will extend along the length of the strip sensor. As used herein, the terms "outer", "outward", "lateral" and derivatives thereof refer to the general direction defined by a vector originating at the longitudinal axis of the sensor array and extending horizontally and perpendicularly thereto. Conversely, the terms "inner", "inward", and derivatives thereof refers to the general direction opposite that of the outward direction. Together, the "inward" and "outward" directions comprise the "transverse" direction.

Referring now to **Figure 1B**, a preferred embodiment of a low profile sensor array **10** according to the present invention is illustrated. The sensor array **10** is configured to inhibit the sensor elements' **20** response to compression energy to provide a selective output which represents substantially only the acoustic energy of interest (shear waves having short wavelengths in the acoustic frequency band of interest). Preferably, the sensor elements **20** include two electrically active layers, each of which lies on opposite sides of a neutral layer, such that the voltage output of the two layers produces a signal output responsive to the flexure or

change in the change in curvature of the underlying surface. As such, the sensor array 10 is configured to act as a mechanical filter to filter the sensor's response to compression energy.

Generally described, the sensor array 10 includes a frame 15 and a plurality of sensor elements 20. The sensor array 10 is configured with a center core layer 75 and opposing (PVDF) outer layers 50, 60 which include piezoelectric layers 500 and 600. As shown in Figure 9, each of the (PVDF) outer layers 50, 60 provides a pair of spatially separated electrodes 501, 502, and 601, 602 which define first and second signal voltages 51, 61 with respect to ground 675. As is also shown in Figure 9, each of the outer layers 50, 60 have an external surface 50a, 60b which is electrically tied to the same electrical ground 675. The two opposing outer layer electrode surfaces 501, 502 and 601, 602 are configured to provide separate electrical signal paths (*i.e.*, voltage outputs V_1 , V_2 , respectively) when the sensor 20 is flexed as will be discussed further below. The signal surfaces 50b, 60a are preferably provided by positioning signal traces 22 (Figure 7) on the appropriate surface of the PVDF layer 50, 60. That is, as shown, the inner facing surfaces of the PVDF layers 50b, 60a, include electrical traces formed thereon.

The outer ground plane or surfaces 675 are preferably provided by applying a conductive layer onto the outer faces of the PVDF layers 50a, 60b. For depositing or forming the electrical traces 22, 22' or the ground surface, any metal depositing or layering technique can be employed such as electron beam evaporation, thermal evaporation, painting, spraying, dipping, or sputtering a conductive material or metallic paint and the like or material over the selected surfaces of the PVDF layers 50, 60. The ground plane is preferably formed by applying a continuous metallized surface over the entire outer surfaces of the PVDF layers 50a, 60b to form a continuous shield. Of course, alternative metallic surfaces or techniques can also be employed such as by attaching a conductive mylar shield layer over the outer surface of the PVDF layers 50, 60. Preferably, conductive paint or ink (such as silver or gold) is applied to the PVDF layers as a thin planar layer such that it does not extend above or around the perimeter edge portions of the signal paths of the internal traces 22, 22'.

As shown in **Figure 1B**, the sensor array **10** includes a frame portion **15** with two longitudinally extending side rails, a first side rail **16**, and a second side rail **17**. Preferably, the frame **15** is configured such that the two side rails **16**, **17** are spatially separate along a major portion of the length of the frame **15**.

5 A plurality of sensor elements **20** are positioned intermediate the two side rails **16** and **17** such that each sensor element **20** is attached to at least one of the sides **16**, **17**. Preferably, as shown, each sensor element **20** is attached to only one side, *i.e.*, at a lateral attachment **18** positioned either at the first side **16** or the second side **17**. Further preferably, as shown in **Figures 1A** and **1B**, adjacent
10 sensors are attached to different sides of the frame **15** and the lateral attachments **18** extend substantially about the center of the sensor element **20**. As shown in **Figures 1A**, **1B**, **2**, **3** and **7**, the sensor array **10** includes a first and second signal trace pattern **22**, **22'**. The trace patterns **22**, **22'** are the same and are configured to define two separate but corresponding active sensor electrical signal regions **25**, **26**,
15 **27**, **28**, **29**, **30** and **25'**, **26'**, **27'**, **28'**, **29'**, **30'** across the upper and lower PVDF film layer sensor elements **20**, **20'**. The sensor array **10** is configured such that each corresponding sensor element electrical signal region **25**, **25'**, **26**, **26'**, **27**, **27'**, **28**, **28'**, **29**, **29'** and **30**, **30'** has a separate and corresponding electrical signal path **25a**, **25a'**, **26a**, **26a'**, **27a**, **27a'**, **28a**, **28a'**, **29a**, **29a'**, **30a**, **30a'** respectively,
20 defining corresponding but separate upper and lower signal paths **51**, **61**. As such, the electrical path for each sensor **25a-30a** extends from a sensor element **20** to an electrical termination or electrical connection pad **40**. Although **Figure 1A** illustrates only one PVDF signal layer, the opposing PVDF layer of the sensor array **10** includes another (second or bottom) signal trace pattern **22'** substantially
25 similar to and configured to align with the top external trace **22** pattern shown, including corresponding primed element numbers. That is, upon assembly or fabrication, two of the PVDF layers shown in the left side of **Figure 1A** are disposed on opposing sides of a neutral core **75**.

30 In a preferred embodiment, the electrical traces **22**, **22'** are applied to the respective PVDF outer layer **50**, **60** such as by applying a silk screened conductive ink or paint pattern. The ground plane is preferably provided on each PVDF layer

50, 60 by applying a continuous layer of conductive ink or paint thereon. The core 75 typically includes a neoprene layer with a thin film of adhesive on each side. The PVDF layers 50, 60 are then secured to the core 75 to sandwich the core therebetween. The electrical connections (pin terminations) are made in an external connector and the upper and lower PVDF ground traces or surfaces 50a, 60b are connected to a common ground 675 thereat. See U.S. Patent No. 5,595,188, the contents of which is hereby incorporated by reference as if recited in full herein.

As shown in Figure 5, the sensor array 10' includes a frame 15' which can be configured to provide supplemental structural attachments 21 at selected areas (such as at the ends) to further structurally tie the two sides 16', 17' together to help provide structural strength or positional integrity for the sensor elements on the array 10'. This can be beneficial for sensor arrays 10' which, once sterilized, are enclosed in a sterile underlying adhesive layer and sterile package for shipment and storage, as the sensor array is typically quickly peeled from its packaging during use. The additional mechanical reinforcement can minimize sensor element 20 displacement from the frame 15'.

Figure 5A illustrates another preferred embodiment of a sensor array 10'' according to the present invention. As shown, the frame 15'' includes a single longitudinally extending side or rail 17'' which is preferably widened relative to the dual rail configuration shown in Figure 1B to provide adequate physical separation (to minimize the potential for electrical coupling) of the electrical traces 22b. Of course, the electrical traces 22b will be altered to extend along the single rail 17''.

Figures 2 and 3 illustrate a section view of a preferred embodiment of the low profile sensor array 10. As shown (in sectional view), the sensor array 10 is configured such that the two piezoelectrically active (PVDF) outer layers 50, 60 of the sensor array 10 (including the outer layers of both the frame sides 16, 17 and sensor elements 20) comprise a first material having an associated first thickness while a core or intermediate layer 75 comprises a second resilient material having a second thickness. Figure 9 schematically illustrates the electrical configuration of the sensor element 20 and will be discussed further below. The external traces 22,

22' are positioned on the respective top and bottom surfaces 50b, 60a (i.e., the interior surfaces on a completed array assembly) of the outer layers 50, 60.

As shown, the core 75 thickness is greater than the thickness of the outer layers 50, 60. In a preferred embodiment, the core 75 is an order of magnitude thicker than the outer layer thickness. More preferably, the core 75 has a depth or thickness of about 600 microns while the outer layers 50, 60 are about 30 microns thick. It is also preferred that the core material be selected such that it has a relative permittivity which is less (and more preferably much less such as an order of magnitude less) than the relative permittivity of the outer layers 50, 60. In one embodiment, a suitable core relative permittivity value is about 5 or 6.

It is also preferred that the core material 75 be selected such that it is resilient or compliant (substantially incompressible material) and preferably has low viscous losses. "Resilient", as used herein, means that the core is sized and formed of a material which allows the sensor array (at least the sensor element) to be conformal to the underlying surface when in position. Stated differently, the core 75 is configured such that at least the sensor elements 20 are substantially compliance matched with the body, i.e., to follow the shape of the underlying patient skin surface when positioned thereon. Preferred core materials include nitrile, neoprene, latex, polyethylene, or high-density polyethylene forms. In a preferred embodiment, the core material is neoprene. Alternatively, the core 75 can be formed as a thin layer of insulator (a neutral center), allowing the two opposing electrically active layers 50, 60 to be electrically separated and directly responsive to the flexure of the underlying surface.

In a preferred embodiment, the core 75 has a first relative permittivity and the outer layers 50, 60 are first and second pliable material layers which have a second relative permittivity. The first relative permittivity is less than the second relative permittivity. As such, the resulting capacitance of the core 75 may be such that it is about an order of magnitude less than the PVDF layers 50, 60. In a preferred embodiment, the core 75 is sized to have a greater thickness than the PVDF layers 50, 60. The core 75 capacitance is related to the material and configuration of the core 75. More particularly, the core 75 capacitance is related

to the core material permittivity (ϵ), and the core configuration (area (A), and the thickness (l)) as stated by the equation ($C=\epsilon A/l$). In a preferred embodiment, the sensor 20 is configured such that the capacitance of the core 75 is less than that of the electrodes defined by the PVDF layers 50, 60.

5 Referring to **Figures 2, 3 and 9**, the outer layers 50, 60 are formed from a piezoelectrically active material such as, but not limited to, polyvinylidene fluoride (PVDF) or its copolymer with trifluoroethylene (PVDF-TrFe). As shown in **Figure 9**, electrodes 501, 502, 601, 602 are formed on both sides of the major surfaces of piezoelectric film 500, 600. In this way, the PVDF material provide
10 outer layers 50, 60 which function as electrodes which can act as an electromechanical transducer and, as such, can be used as an acoustic sensor 20. Generally described, and as shown in **Figures 14A, 14B, and 14C**, the sensor 20 is configured such that when the piezoelectric material is subjected to strain or stress (flexure or curvature displacement) an electric potential or voltage proportional to
15 the magnitude of the strain or compression is developed across the thickness of the piezoelectric material. *See e.g.*, U.S. Patent Application Serial No. 08/802,593, the contents of which is hereby incorporated as if recited in full herein. A preferred electrical configuration will be discussed further below.

Figure 4 is a side view of a low profile sensor array 10 according to a
20 preferred embodiment of the present invention. As shown, the sensor array 10 is configured such that each of the sensor elements 25-30 and the frame 15 are in (substantially) coplanar alignment along at least the top surface 10a of a major portion of the frame 15 region when viewed from the side (*i.e.*, the sensors 20 and sides 16, 17 have the same material thickness and layers). More preferably, as
25 shown, the sensor array 10 (and the sensor array 10'' with the single rail frame 15'') is configured such that the elements 20 and the frame 15 have the same profile configuration along the top and bottom surfaces 10a, 10b. The sensor array 10 is substantially flush across the top and bottom surfaces 10a, 10b. As shown, the linear strip array preferably includes a top and bottom outer surface 10a, 10b
30 with a substantially constant and flat profile. Alternatively, as will be discussed further below, the top outer surface can include one or more discrete masses 900 or

stiffeners 910 attached to the sensor element region to modify the response of the flexural sensor element 20 (Figure 26).

Figure 5 shows an alternate embodiment of a sensor array 10'. In this embodiment, the lateral attachments 18' extend about alternating forward and rearward edges of the sensor elements 20. Also as shown, the sides or side rails 16', 17' have a greater lateral length, providing additional area for the signal traces 22. The additional area can allow the separate paths to be spatially separated by a greater separation distance or can allow additional sensor elements 20 to be used (more area used for additional traces needed for the additional elements). The additional width of the sides 16', 17' can also help minimize electrical cross talk along the length of the signal path. Similarly, Figure 5A illustrates a single-rail embodiment of a sensor array 10'' according to the present invention. As shown, the sensor arrays 10, 10', 10'' include a plurality of sensor elements 20 (preferably more than four sensor elements, and more preferably six or more sensor elements).

Turning now to Figure 6, a preferred structural foundation layer 100 is shown. The foundation layer 100 provides the structural foundation for the signal traces 22, 22' which are preferably applied to the PVDF layers 50, 60 and attached to the foundation layer 100, as will be discussed further below. As shown, the foundation layer 100 defines the frame 15, the side rails 16, 17 and the pads for the sensor elements 20. It also includes a neck portion 102 which separates the frame upper portion which includes a resilient core material to a thinner ribbon portion 105 (which extends down to the terminal connection ends at the connector (not shown)). In any event, the neck portion 102 of the frame 15 is preferably configured to transition the sensor array from one thickness to another such that the core 75 has a first thickness at the neck upper portion 102 but substantially terminates prior to the end of the neck lower portion 105 to a second reduced thickness. Preferably, as shown in Figure 6, the sensor array 10 is configured such that the neoprene extends down until the area shown in cross hatch. A preferred neoprene stop zone 76 is shown at position A-A. Preferably, the ribbon 105 is configured such that the PVDF electrically active surfaces do not contact. For example, other thin insulating core materials such as a double sided polyethylene

film can be positioned such that it extends between the two inwardly facing surfaces of the PVDF layers 50, 60.

Figure 7 illustrates a preferred trace pattern 22, 22' which is, upon assembly, positioned onto the appropriate surfaces of the film layers 50, 60 forming the respective electrical regions for the sensor elements 25-30, 25'-30' and respective signal paths 25a-30a, 25a'-30a' which extend down the neck portion 102 and ribbon portion 105 of the sensor frame. As shown in Figure 7, the electrical pattern 22, 22' includes a sensor pad active region 220 and linear traces 221. The trace pattern is disposed onto the piezoelectric layers 50, 60 as described above. Preferably, it is formed by applying conductive ink, such as disposing onto the outer surfaces of the outer layers 50, 60 a silver ink silk screen pattern. While particular conductive patterns are illustrated in Figures 7 and 5A, alternative conductive patterns may also be used. For example, conducting paint, flex circuits, foil or other coating or metal deposition methods and techniques may also be employed. It is preferred that, if flex circuits are used, that they are configured or attached to the foundation layer 100 so as to be transparent to the structure of the sensor array to minimize any potential interference with conformance of the sensor element to the body.

For clarity, it will be understood that, according to the present invention, protective films or coatings may also be positioned over the PVDF "outer" layers forming the ground and signal planes (or traces) as long as they are applied so as to be substantially transparent to the operation of the sensor elements. Therefore, as used herein, the trace(s) 22, 22' or outer layers 50, 60 can include traces or layers which are covered with moisture barrier coatings, adhesives, or other materials and are thus not truly "external" or "outer" as described for ease of discussion herein.

Figure 8B is an enlarged view of a sensor element 20. Preferably, the sensor element 20 is substantially rectangular with side dimensions of from about 8 mm to about 11 mm. In a preferred embodiment, as shown in Figure 9, the upper and lower traces 22, 22' are deposited onto the inwardly facing major surfaces of the (PVDF) layers 50, 60. As such, the electrically active regions defining the signal paths include the pad regions 25, 25' and the signal lead paths 25a, 25a'

which are spatially separated a distance from top to bottom about a central neutral core 75. The PVDF outer layers 50, 60 are preferably relatively thin (such as below about 60 microns, and preferably about 30 microns) while the core depth 75 a is an order of magnitude greater (above 300 microns, and more preferably above about 500 or 600 microns). This configuration makes the thickness of the PVDF layer 50, 60 relatively structurally negligible compared to the depth or thickness of the core 75. As shown in Figure 9, the upper and lower signal paths 502a, 602a defined by the trace patterns 22, 22' are separated by a distance which is substantially equal to the core depth 75a.

Figure 10 schematically illustrates a preferred configuration of a low profile sensor array assembly 120. As shown in Figure 10, the sensor array assembly 120 includes four laterally positioned linear sensor or strip arrays 120a, 120b, 120c, 120d in electrical communication with a signal processor 150 (having an opto-isolator 151). Figure 10 illustrates four sensor arrays 10 positioned over preferred intercostal spaces. See pending PCT and U.S. Patent Application Serial Numbers identified as Attorney Docket Nos. 9023-15IP.WO and 9023-15, 16), the contents of which are hereby incorporated by reference as if recited in full herein. Figure 10 also illustrates a preferred pigtail arrangement for the sensor array assembly 120. As shown, the pigtail 120P preferably extends off the sensor elements toward the sternum of the patient, thereby allowing standard cord sizing notwithstanding the access to the patient (i.e., whether the system must be hooked to the patient from the right or left hand side of the bed). Alternatively, as shown in Figure 11, the electrical pigtails 120P can extend from the opposing side.

Similarly, Figures 11 and 12 illustrate a preferred low profile sensor array 120 assembly positioned on a subject which comprises four linear array sensors 10, the sensors having six sensor elements 20 each. Of course, alternative numbers of sensor arrays 10 or sensor elements 20 on the arrays 10 can also be used (either in combination or alone). Figure 12 illustrates the low profile acoustic sensor array 10 positioned on the skin 200 of a patient over an acoustic window above the cardiac region of interest. Thus, the sensor array according to the present invention preferably includes means for releasably securing the sensor array to a patient.

Such means may comprise an adhesive layer which may be incorporated in or applied to one side of the sensor array such as the adhesive layer 775 shown in **Figure 9**. Suitable adhesives for releasably securing medical apparatus or devices to a patient are known to those of skill in the art. As shown in **Figure 9**, the sensor array 10 also preferably includes a release adhesive 775 positioned along a major portion of the lower external surface 60b to secure the sensor array to a patient during clinical use. Of course, sterile adhesive creams, double-sided tapes, and the like can alternatively or additionally be used to position the array on the patient's skin.

Turning now to **Figures 9, 13A, 13B, and 14A-C**, preferred electrical and operational schematics for the sensor elements 20 are shown. As discussed above, **Figure 9** illustrates the piezoelectric active outer layers 50, 60 as including a PVDF (or other piezoelectric polymer) portion 500, 600 and two corresponding opposing first and second interior active electrode surfaces or layers 501, 502 and 601, 602. The interior film surfaces 502, 602 each include a separate electrical signal path 502a, 602a while the outer film surfaces 501, 601 are tied to a common ground 675.

Figures 9 and 13A-B illustrate that the PVDF is disposed on the first (upper) outer layer 50 with a polarity of negative to positive. That is, the major inner surface 50b has a positive polarity while the major outer surface 50a has a negative polarity. In contrast, the PVDF is disposed on the (lower) outer layer 60 with the reverse polarity; positive on the major inner surface 60a, and negative on the major outer surface 60b. Of course, the layer polarities could also be reversed (*i.e.*, the upper layer 50 can have negative to positive while the bottom layer 60 can have positive to negative).

As shown in **Figures 14B and 14C**, each of the outer layers 50, 60 provides a voltage (V_1 and V_2) 51, 61 in response to flexure of the sensor 20, respectively, even in response to long compressional waves. However, in response to gross translation of the sensor 20 which does not result in flexure, no voltage will result. Because the polarities are reversed, and because the core material and sensor configuration provides a high degree of coupling between the two outer 50, 60

active (electrical) layers, the absolute value of the voltages for a particular flex or curvature will be substantially the same. However, because during flexure or curvature of the sensor, one layer is in compression and the other layer in tension, the sign of the voltage will be opposite between the two layers. Further, if movement of the sensor does not result in curvature of the sensor, then the polarity of the sign will be the same between the two layers. Thus, the instant sensor configuration is preferably configured to read the voltage differential of the two voltages, that is the difference between the response voltages V_1 , V_2 .

Advantageously, as shown in Figure 13a, the electrode configuration is such that the sensor 20 acts like a differential amplifier 63. In operation, the sensor array 10 takes the voltage differential of the two response voltages V_1 , V_2 to generate a signal response which has an increased voltage value (approximately doubled value) and, thus, can provide improved SNR performance. Further, for non-flexure sensor excitation, the voltage polarities are such that the signal responses from each layer 50, 60 cancel each other, minimizing signal output for non-flexure excitations.

Thus, in operation, as schematically shown in Figure 14a, for a non-strain input such as a compression wave (typically input to the sensors by ambient noise that is carried by noise in the air, or noise that is transmitted through structural vibration), both the top and bottom sensor layers see the same force, and without a strain or flexure to cause a curvature in the layers 50, 60 the polarity of the voltages are such that any signal response is cancelled and no signal output is transmitted for detection. In contrast, as shown in Figure 14b and 14c, the polarities of the layers 50, 60 associated with the strain in the PVDF or outer (electrical response) layers 50, 60 have opposing polarities. For example, for a given flexure in the outer layer 50, and a (V_1) response of 2 microvolts, the (V_2) response may be about (-2 microvolts), and the signal response for this flexure will then be $2 - (-2)$ or 4 microvolts. Of course, the magnitude of the voltage will vary according to the degree of strain or curvature of the flexure.

Figure 14a illustrates the substantial non-response associated with a compression or longer wavelength transmitted across the sensor situs while

Figures 14b and 14c show the voltage response (opposing polarity) corresponding to flexure at shorter wavelengths of interest. As shown, the voltage polarity corresponding to an upward flexure is positive for the upper PVDF layer **50** and negative for the lower PVDF layer **60** and the polarities reverse for a downward flexure.

In a preferred embodiment, as schematically shown in **Figure 14d**, the sensor arrays **10, 10', 10'', 10'''** are configured such that they are selectively responsive to shorter wavelengths **310** that cause flexure through the thickness of the sensor element **20, 420**, while being substantially non-responsive or resistant to longer acoustic wavelengths **300**. The longer wavelengths **300** are typically associated with compression waves in the body or in the ambient noise within the examining room, and which cause compression through the thickness of the sensor element. In operation, due to differences in the speed of the waves or a frequency band of interest, shear waves typically have much shorter wavelengths than the wavelengths associated with compression waves. Stated differently, the sensor is responsive to the flexural mode of displacement caused by short wavelengths of shear waves **310**, and substantially non-responsive to acoustic inputs of the much longer compression wavelengths **300**. At the same time, the sensor array is configured to respond to shear waves having shorter wavelengths **310**. Thus, the sensor array **10** of the present invention acts as a mechanical filter and inhibits or minimizes the sensor elements from generating a detectable signal response for long wavelengths at frequencies of interest. The sensors and sensor arrays described herein include an operational range for the acoustic wavelengths of interest for the diagnosis and detection of coronary artery disease. Preferably, the sensors include an operational range of at least about 100-2500 Hz, and more preferably a range of about 100-1000 Hz. Preferably, the sensor elements **20** are configured and sized on the frame **17** to respond to shear waves at the operating frequencies of interest such as those characterized as having propagation velocities of less than about 25 m/s, or more in the range of about 5-15 m/s, and to suppress or inhibit signal response for compressional waves or acoustic waves having a propagation velocity above about 100m/s. More preferably, the sensor is

configured to suppress response associated with the wave speed of compressional waves in the air, typically a velocity of about 340 m/s and the response associated with the wave speed of compressional waves in the body, the compressional wave velocities being typically about 1540 m/s in the body.

5 **Figure 8A** illustrates an alternative discrete or single sensor embodiment of the present invention. The signal return covering the back of the film has been removed for clarity. It is preferred that the width of the pigtail be configured and sized to hold the capacitance of a signal trace below about 10% of that of a sensor element. As shown, the single sensor **201** includes a positive signal **280** and
10 negative signal **281** electrical path which is formed by the two PVDF layers **50j**, **60j** similar to the electrical traces **322,322'** formed onto the outer PVDF layers of the strip array **10** discussed above. As shown, the single element **201** can be formed by configuring four signal lines on a single sheet of PVDF material. The single sheet is configured to be folded, such as along the dotted fold lines shown,
15 to provide the two interior signal paths **280, 281** and the external common ground. The two grounds **290a, 290b** are preferably formed by a metallized mylar shield **290** configured to provide a continuous planar electrical shield on one surface of the PVDF material (the surface opposing the electrical traces **322, 322'**). The electrical pin out can also be alternatively configured as will be appreciated by one
20 of skill in the art.

Figures 17A and 17B illustrate yet another preferred embodiment of an accordion pleated sensor array **10'''** which can advantageously minimize mechanical vibration and cross-talk between sensor elements **421, 422, 423** and their associated transmission lines **431, 432, 433** while also providing a mechanical
25 filter (to reject compression energy and allow selective acoustic response as discussed above) according to the present invention. This low profile acoustic accordion array is also configured to selectively respond to shear waves while rejecting compression wave energy in the frequency range of interest. As shown, this sensor array **10'''** includes multiple discrete or unitized sensors **420** and
30 corresponding individual transmission lines **430** which are electrically connected at a primary connector **450** and into the signal processor operating system **150I**. As

shown in **Figure 17B**, the sensor array 10''' preferably includes three sensor elements 421, 422, 423 with corresponding transmission lines 431, 432, 433. The separate transmission lines 431, 432, 433 can substantially isolate each element and respective transmission line to thereby minimize the cross talk between adjacent sensor elements.

As is also shown in **Figure 17B**, the transmission lines 431, 432, 433 are preferably folded or formed with a series of undulations 435 along the length of the transmission path (the transmission path extending between the sensor element 420 to the primary connector 450). Although shown as formed with accordion type "sharp" creased or crimped edges ("pleats"), it will be appreciated by one of skill in the art that other mechanical damping configurations may also be used. For example, but not limited to, the transmission line can be formed with a series of sinusoidal curves or waves or folds formed along a portion of its length, or formed with alternating material widths (*e.g.*, thin to wide, wide to thin), or a combination of fold or curve patterns, interposed extra material or alternating material composition, weight, and the like. As used herein, the term "undulating" includes the above mechanical damping configurations.

Figures 17A and 17B illustrate a preferred sensor array 10''' alignment. As shown, in position on a subject, the sensor array 10''' positions the sensor pads 421, 422, 423 such that the discrete sensor pads are configured as an array 10''' with a plurality of unitized, separated, or discrete sensors; that is, the sensors 421, 422, 423 and corresponding transmission lines 431, 432, 433 are configured as discrete aligned segments in the array, *i.e.*, they have "unitized separation". As shown, the rear of the sensor pad 423b of the most distal sensor 423 (the sensor positioned closest to the center of the subject's chest) is proximate to the front 422a of the next adjacent sensor pad 422. The rear of that sensor pad 422b is positioned proximate to the front 421a of the next sensor pad 421. Further preferably, as shown, the sensor pads 421, 422, 423 are positioned such that they are substantially linear arranged and symmetrically extend relative to a horizontal or lateral alignment axis A-A. Further, it is preferred that each of the sensor pads is conformal to the underlying skin and the transmission lines are sized and

configured such each is spatially separated from the others (*i.e.*, non-contacting with the others).

The transmission line **430** preferably longitudinally extends off one end portion of the sensor pad (shown as the rear portion) **423b**, **422b**, **421b**. Preferably, the sensor array **10'''** is configured and sized such that the transmission line for each sensor **430** extends off the sensor pad in a manner that, when connected to the system connector **450** and securely attached to the surface of the patient, the transmission line **430** defines a concave contour along a portion of its length when viewed from the side. That is, as shown by **Figures 17A and 17B**, the length of the transmission line **430** is such that it is sufficiently long when in position so as to provide a suitable amount of slack to prevent tensioning of the transmission line when the primary connector **450** is connected to the signal processing input port **150I**. In addition, as shown, the sensor array **10'''** is configured such that the array includes three discrete sensors **420**, and each sensor **420**, sensor pad **421-423**, and associated transmission line **430** is a substantial mirror image of the other sensors, sensor pads, and transmission lines. However, the sensor array **10'''** can include alternative numbers of sensors such as 2, 4, 5 or more. In addition, the system can employ several of the multi-element sensor arrays **10'''** (such as four) of the tri-sensor discrete element sensor array **10'''** (not shown). This plurality of three element sensor arrays **10'''** can reduce the number of patient interconnections undertaken by a technician at patient application in order to prepare the equipment for use, while still allowing twelve individual sensor pad elements to be used for more precise acoustic detection on a patient.

Figure 17A also illustrates a reflector **424** positioned on each of the sensor elements **420** to facilitate the detection system's photogrammetric recognition of the positional alignment of the sensor elements **420** when on the body. The reflector **424** can be applied by various means such as via reflective paint or by attaching reflective tape to the external (exposed) surface of the sensor element **420**. See *e.g.*, co-pending and co-assigned U.S. Patent Application identified by Attorney Docket No. 9023-11IP, to Van Horn, entitled "*Methods, Systems, and Computer*

Program Products for Photogrammetric Sensor Position Estimation." The contents of this disclosure are hereby incorporated by reference as if recited in full herein.

Referring now to **Figure 18A**, the sensor array **10'''** is shown in a pre-use position (not positioned on a subject). Each sensor **420** includes a sensor pad **420p** and a termination end **440**. The termination end of the sensor **440** is connected to the primary connector **450**. In a preferred embodiment, a mechanical termination stiffener **441** is applied over the termination ends **440** adjacent the primary connector **450** to help stiffen and support the relatively thin ends of the sensors **420**. Preferably, the termination stiffener is formed of a non-conducting material such as a transparent film or the like. Suitable materials include polyester and/or polystyrene and the like. Also preferably, each sensor **420** has a discrete or unitized termination stiffener **441** which is spatially and mechanically separate from the others to help isolate each of the signal paths from the others. The termination stiffener helps provide sufficient structure for the relatively thin flexible PVDF body **420b** (**Figure 20A**) onto which the connector or end terminations can be attached. Of course, alternate structural enhancing means can also be used as will be appreciated by those of skill in the art.

As shown in **Figures 18A** and **18B**, the transmission lines **430** each include a plurality of undulations or pleats **435** formed along the length thereof (typically under about 23 cm). Preferably, each transmission line **430** is configured the same as the others. In a preferred embodiment, as shown, each transmission line **430** preferably includes at least four undulations or pleats **435** serially formed in continuous repeating (non-interrupted) fashion along a major portion of the length thereof. Of course, as will be appreciated by one of skill in the art, the number of pleats, the shape, and the pattern or configuration of same can be alternatively arranged. The undulations or pleats **435** positioned along the transmission lines **430** help to isolate the transmission paths so as to minimize the sensor array's **10'''** reaction to unwanted acoustic inputs between adjacent elements or lines or even from vibration from a computer or processor or data system connected to the array for receiving the data signals associated with the flexure responsive generated signals. In another preferred embodiment, the pleats **435** or undulations begin

substantially immediately after the sensor pad **420p** and extend continuously about every 0.5 inches or 1.25 cm (0.5 inches or 1.25 cm edge to edge) along the length of the transmission line **430** until the termination end of the sensor **440**.

5 It is also preferred that the electrical lead lengths of the transmission lines **430** and each of the sensor pads **420p** are maintained as a constant size and length to allow for the differential sensing capability such as discussed under the section describing the other sensor array configuration above.

Referring now to **Figures 19A** and **20A**, a preferred embodiment of a sensor body **420b** is shown. Similar to the embodiment shown in **Figure 8A**, the
10 sensor body **420b** includes a thin layer of piezoelectric film **420f** ("PVDF") having opposing first and second major surfaces **420f_a**, **420f_b**. The first major surface **420f_a** of the film includes an active metallized electrode surface **22e** defining the opposing sensor pad regions **420p1**, **420p2**. The first major surface **420f_a** also includes the separate electrical traces **480**, **481**. Preferably, the electrical traces
15 outside the electrode regions are inactive, for example, by the trace regions not being initially polarized, or depolarized such that they act to carry or transmit flexure signal generated by the electrode sensing regions.

The second major surface **420f_b** of the PVDF film layer **420f** (the surface underlying the exposed surface shown in **Figure 19A**) is formed from a conductive
20 trace such as a conductive ink (but of course other methods for disposing a conductive trace can also be used such as those described hereinabove). As shown in **Figure 19B**, the second major surface **420f_b** is preferably configured to provide a continuous conductive active surface pattern **22e'** which includes the upper portion of the "T" defined by the two pad portions of the sensor body **420p1**,
25 **420p2**. The second major surface **420f_b** also includes a trace **438g** positioned along one side of the (PVDF film). This third transmission line or trace **438g** acts as a ground signal path or line.

In a preferred embodiment as shown in **Figure 19B**, the trace **438g** is preferably configured to extend a greater distance on the termination end of the
30 sensor **440** and thus form the long finger portion **440f** of the termination end of the sensor. This additional length allows this portion of the sensor to be folded over to

the other side of the sensor to align the ground signal line **438g** with the signal transmission lines **438b**, **438c** for each of the electrodes **450**, **460**. As shown in **Figures 21B** and **22**, this termination configuration provides a four point termination, one each associated with the electric shield "ground" **438a**, the PVDF film layer traces **438b**, **438c**, and the folded **438g** ground trace. The four-point termination connection for the primary connector **450** is thus configured on a single common connection surface.

The PVDF film layer **420f** defines the acoustic sensor signal paths **480**, **481**, and ground signal path **438g** for each of the sensor pads or electrodes **450**, **460**, including the active portion of the sensor pad **420p1**, **420p2** and the associated transmission or signal paths **438b**, **438c**, **438g**. Similar to the operation of the differential sensor **63** explained for **Figure 13** and **13A**, the PVDF film **420f** is preferably configured to provide opposing sensor pads **420p1**, **420p2** which act as electrodes **450**, **460** having opposing polarities. As shown in **Figure 20B**, the negative and positive polarity associated with the upper and lower electrodes **450**, **460** provide the differential configuration for the flexure induced voltages v_1 , v_2 . Of course, as note for the above-described embodiment, the polarities can also be reversed, but the sensor region is preferably configured with opposing polarities for the sensor pad in order to provide the differential based operational sensing configuration. In any event, as shown, the PVDF film layer **420f** is configured to provide an upper electrode surface and a lower electrode surface **450**, **460**, respectively (the lower electrode surface and the surface shown in **Figure 19A** disposed on the patient such that these surfaces face the skin of the patient).

Preferably, as shown in **Figure 20A**, in order to form the sensor assembly **420**, a layer of nonconductive material (such as polyester film) **499** is attached to or applied to overlie substantially the entire length of both sides of the PVDF film layer **420f** along the linear transmission line **430** or trace portion of the sensor body **420b** (excluding both sides of the sensor pads **420p1**, **420p2** or upper portion of the "T" region of the sensor body). Preferably, as is also shown, the polyester film layers **499** end a distance away from the termination end of the sensor **440** -- substantially along a line shown by **P-P** in **Figure 19A** and **Figure 21B**. A single

sided or double sided adhesive-backed polyester tape can be conveniently used to attach the polyester layers to the respective PVDF film surface **420f_a**, **420f_b**. Of course, other adhesive or attachment means can also be used as will be appreciated by one of skill in the art.

5 The sensor body **420b** also includes a resilient core **75'** which is applied to one side of the sensor pad region of the sensor body **420b** as shown by the arrow associated with the core element **75'** drawn in dotted line in **Figure 19A**. **Figure 20A** also shows the preferred assembly position of the core **75'** relative to the sensor pad **420p2** region of the sensor body **420b**. In position, the core **75'** is positioned to overlie and attach to the sensor pad **420p2** (such as via an adhesive).
10 As shown in **Figure 20A** in double-dotted line, to form the flexure-responsive sensor element **421-423**, the PVDF film sensor pad **420p1** is folded over the central core layer **75'** to overlie the opposing PVDF film sensor pad **420p2** as shown in cross section in **Figure 20B**. The folded configuration of the sensor **420**
15 (that is preferably only the sensor pad region is folded) is shown in **Figures 18A** and **18B**.

 As is also shown in **Figure 20A**, in this embodiment, first and second layers of conductive shielding material layers **501**, **502** are attached to the sensor body **420b**. In a preferred embodiment, the shielding material layers are metallized
20 film, and more preferably a thin sheet of MYLAR® film. The conductive shielding material layers **501**, **502** help to shield the sensor **420** to minimize the introduction of electromagnetic interference into the sensor signal paths. As shown in **Figure 20A**, the shielding material layers **501**, **502** are sized and configured so that they do not contact along the sensor pad region of the sensor, *i.e.*, the
25 perimeter edges of the sensor pad are not enclosed by the shielding material layers **501**, **502** when the PVDF film sensor pads are aligned over the core **75'**.

 As shown in **Figure 20A**, the first shielding layer **501** linearly extends from the upper neck portion of the sensor body to an end portion which is adjacent the termination end of the sensor **440**. In this embodiment, the first shielding layer
30 does not extend to cover the PVDF sensor pad regions **420p1**, **420p2**. As is also shown, the first shielding layer **501** ends at substantially the same position as the

polyester layer 499 but also includes a termination protrusion end 438a which longitudinally extends a further distance to align with the active signal transmission lines 438b, 438c.

5 **Figure 21A** shows the preferred end point for the non-conducting layers 499 and the upper shielding layer 501. As shown, the material extends adjacent but below the sensor pad regions 420p1, 420p2. **Figure 21B** shows the outer shielding material layer 501 positioned on the PVDF film layer 420f. As noted, the shielding layer 501 and the intermediately positioned polyester layer 499 end at a common termination line P-P for a major portion of the outer shielding material
10 layer 501. This configuration allows electrical access for the signal lines 438b, 438c. This configuration also allows for electrical engagement with the ground path 438g when it is folded up to contact the shielding material layer 501.

As shown in **Figure 20A**, the second or opposing outer shielding layer 502 is configured and sized to substantially conform to the shape and size of the
15 unfolded PVDF film layer 420f. As such, it includes a "T" shaped body of which the upper portion is preferably folded along with the sensor pad 420p1. When folded, the second shielding layer 502 provides a continuous electric shield for the exposed major surfaces of the sensor pad 420p and also preferably ends into or contacts the upper portion of the first shielding layer 501a at a lower edge 502a.
20 Accordingly, the two opposing shielding layers 501, 502 provide a contiguous shield for the sensor 420 as shown in **Figure 17A** while the insulating polyester film layer maintains the electrical integrity of the internally disposed signal paths 438b, 438c. Similar to the first shielding layer 501, the second shielding layer 502 also includes a longitudinally extending protrusion portion 438a' positioned to
25 overlie the first protrusion 438a with the PVDF film layer 420f disposed therebetween. Upon termination into the connector, the protrusion portions 438a, 438a' provide the electrical continuity for the shield layers 501, 502.

Figure 22 illustrates the electrical signal paths 438a, 438b, 438c, and 438g formed onto the sensor body 420b. The live signal paths with opposing polarity
30 are 438b and 438c, while the ground is provided by 438g and the shield by 438a, 438a'.

Advantageously, as shown in **Figure 20b**, the electrode configuration **450**, **460** is such that the sensor **420** acts like a differential amplifier **63'** as discussed for the embodiment described above. In operation, the sensor **420** takes the voltage differential of the two response voltages v_1 , v_2 to generate a signal response which has an increased voltage value (approximately doubled value) and, thus, can provide improved SNR performance. Further, for non-flexure sensor excitation, the voltage polarities are such that the signal responses from each layer **450**, **460** cancel each other, minimizing signal output for non-flexure excitations.

Preferably, the sensor component materials such as for the core are selected and configured as described for the first embodiment described herein.

As shown in **Figure 23**, the sensor array **10'''** preferably includes a structural support or carrier member **600** which is positioned over the exposed side of the plurality of sensors **420** (the side away from the patient when in operable position). The carrier member **600** is release-ably secured to each of the plurality of sensors **421**, **422**, **423**. Thus, the carrier member **600** is used to maintain the sensor elements **421**, **422**, **423** in a predetermined alignment so that an operator or technician can remove the sensor array from a shipping package, attach the discrete sensor elements **421**, **422**, **423** onto the patient, and strip the carrier member **600** away, conveniently providing unitized installation for discrete sensors. The underside of the sensor elements **421**, **422**, **423** preferably includes a layer of adhesive which is configured to securely attach the sensor's in position on a patient during use as described for the first embodiment above (of course, the adhesive can be directly applied to the patient instead). The carrier member **600** conveniently allows the technician or operator to easily position the discrete individual sensor elements **421**, **422**, **423** onto the patient while maintaining the preferred alignment positional relationship therebetween. Thus, the carrier member **600** is configured to be temporarily attached to the sensor elements **421**, **422**, **423** (only during shipping and patient application, *i.e.*, attached during the time period prior to sensor operation). Advantageously, the carrier member **600** can limit the number of installation steps the operator must take to prepare the patient for acoustic evaluation. Further, the carrier member **600** is configured to release or detach from

the sensors 421, 422, 423 once the sensors are secured to a patient. Of course, this carrier member can also be used with other flexible low profile sensor arrays to help facilitate the positional and structural integrity while applying same to the patient.

5 This disengagement is preferably accomplished by disengaging an edge portion of the carrier such as an exposed tab 601 and pulling the carrier member 600 away from the sensor elements 421, 422, 423 without disturbing the installed position of the sensors on the patient. Advantageously, the carrier member 600 provides the installation convenience of structurally related sensors while also
10 allowing the structural isolation of the sensors during operation.

Figure 27 schematically illustrates the preferred product configuration with the releasable carrier member 600. Step 1 includes a first carrier member 600 and a second carrier member 619 used during transport or shipment to a use facility (step 1). As shown, the second carrier member is an easily releasable (low peel
15 strength) tape or the like which is used to protect and maintain the patient-adhesive material intact during shipment. Step 1 also shows that prior to use, the second carrier member is pulled away and released exposing the bottom of the sensor elements and the adhesive thereon. Step 2 illustrates that, once the sensor elements are secured to the patient, the top carrier member 600 can be pulled away leaving
20 the sensor elements exposed. Thus, the top carrier member 600 preferably has a peel strength which is less than the bond strength of the adhesive/patient attachment. The top surface of the sensor elements can also include discrete masses or reflectors as will be discussed further below. Step 3 illustrates the positional alignment of the sensor elements 420 provided by the fixed structural relationship via the top carrier member 600 during positioning onto a patient.
25 Thus, conveniently, once the top carrier member 600 is stripped away, the sensor elements 420 are in position and ready for acoustic operation. The carrier member 600 is particularly helpful for discrete element sensor arrays 420, but the present invention is not limited thereto, and can of course, be employed with the strip array
30 10 embodiment described herein.

Another preferred embodiment of the present invention includes a sensor array 10'''M as shown in **Figure 24A**. In this embodiment, at least one discrete mass 900 or external flex stiffener 910 is added to the upper (exposed when on a patient) surface of each sensor element 420. This configuration can modify the flexural response of the sensor element 420 and may improve the coupling of the sensor. Preferably, the discrete mass 900 or external stiffener 910 extends across at least a portion of the short dimension of the sensor element. It is also preferred that the mass (or stiffener) be sized and configured on the sensor element 420 such that it is locally discrete as opposed to distributed (distributed meaning extending continuously across the long dimension of the sensor element).

In a preferred embodiment, as shown in **Figure 24A**, a centrally positioned discrete mass is positioned on each sensor element 420. Preferably, the mass is formed from a high-density material such as a tungsten alloy, lead, or other heavy metal. A suitable discrete mass 900 weighs about 3-6 grams, and more preferably about 4.5-5 grams. Typical dimensions of the discrete mass is about 0.2x 0.2 x 0.42 inches (or about a 5mm length across the short dimension of the sensor pad). Examples of discrete external stiffeners include a layer of material having a different (more rigid) stiffness as compared to the PVDF layers or the core.

Figures 24A-E, 25A-C, and Figure 26 illustrate exemplary discrete mass and stiffener configurations according to the present invention. **Figure 24B** illustrates a plurality of discrete masses 901 positioned on opposing ends of the sensor elements 420. **Figure 26** illustrates a discrete mass 900 positioned on the strip array 10. **Figure 24C** illustrates a discrete mass 900 positioned on the sensor element 420 and a discrete mass 900 and a second discrete mass 900a positioned on the transmission path 430. **Figure 24D** illustrates a plurality of discrete masses 900 positioned onto the sensor pad 420. **Figure 24E** shows a plurality of alternately configured discrete elements 902 positioned on the sensor element 420. **Figure 25A** illustrates a pair of opposing external stiffeners 910 positioned onto the sensor element 420 while **Figure 25C** illustrates a single center stiffener 910. **Figure 25B** shows that the stiffener 910 can be combined with a discrete mass 900.

The reflectors (424, **Figure 19A**) or a reflective material can also be conveniently applied to the exposed surface of the stiffener 910 or discrete mass 900 to facilitate system positional operational alignment as discussed above.

5 Additionally, the stiffness of the sensor element 20, 420 can be adjusted by selecting the core materials to provide a different more stiff resilience at one or more regions in the pad such that the stiffer regions extend in at least one region across at least a portion of the short side of the sensor.

Fabrication

10 As shown, in **Figures 1A and 1B**, in a preferred embodiment, the sensor array 10 is fabricated as a unitary body. That is, unlike conventional sensors, there is no requirement to assemble discrete sensor elements onto an underlying electrical ribbon. Preferably, at least the frame 15 and sensor elements 20 are configured as a unitary body, and more preferably, the sensor array itself 10 is an
15 entirely unitary body (*i.e.*, a single piece construction comprising multiple layers but no discrete components excepting an electrical interface connector (not shown) which is adapted to be engaged with the electrical terminations 40).

For the embodiment shown in **Figure 17A**, it is preferred that the core 75' be extruded, molded, formed, or cut, and that after the electric shield layer and
20 other layers are positioned (and the sensor pad folded), the undulations be formed by mechanically crimping the assembled sensor at desired spacings along its length. Of course, other crimping means or forming means such as specialized tooling can also be used to configure the undulations onto the sensor body as will be appreciated by those of skill in the art.

25 **Figure 16** shows a block diagram describing a preferred method of fabricating a low profile sensor having two separate PVDF layers according to the first described embodiment. After the foundation or core is formed (*i.e.*, such as cut or extruded), the outer layers 50, 60 are attached thereon to form the strip sensor (**Block 300**). The foundation layer is cut so that a series of proximately
30 located and non-contacting pads are formed onto a frame segment in the foundation layer (**Block 310**). An electrical signal path is positioned onto each of

the outer layers (PVDF film) which is then secured to the foundation layer (**Block 330**).

Optionally, the PVDF film may be selectively activated, *i.e.*, only selected regions such as the sensor pad regions are actively polarized. Alternatively, selected portions of the PVDF film may be substantially deactivated by applying heat thereto (**Block 350**). As will be appreciated by those of skill in the art, in order to appreciably enhance the piezoelectric effect in the PVDF material, the material is typically exposed to an appropriate electrical poling potential across the thickness of the film for an extended period of time. As used herein the term “selectively activating” or “selectively polarizing” thus means exposing selected regions of the PVDF material to an electrical poling potential to enhance the piezoelectric effect in the film. Thus, during manufacturing, exposing only the sensor pad regions and not the rails can minimize the “active” nature of the rails and/or non-sensing areas of the PVDF film thereby providing substantially “non-active” regions. In addition, as noted above, the entire sensor can be subjected to the electrical poling potential, and then the rails can be “de-poled” such as by heating. Alternately, of course, “selective polarization or activation” is not required. For example, the entire PVDF film employed in the sensor can remain piezoelectrically enhanced or “activated”.

Figure 16A illustrates additional preferred method steps. As shown, the frame segment is formed such that it includes a pair of longitudinal sides and the series of non-contacting pads are arranged to attach to one side of the frame segment (**Block 312**). Preferably, a pattern defining a plurality of electrically separate external traces are disposed onto a surface of each of two PVDF layers (defining a corresponding top and bottom electrical trace which is associated with each of the longitudinally extending opposing sides and the sensor pads) (**Block 335**). Also preferably, as shown by (**Block 340**), the disposing step is performed by applying a conductive layer with a trace pattern such as via conductive ink and the two PVDF layers are attached to the foundation layer such that the signal traces face each other and contact the foundation layer. (**Block 345**).

Preferably, for extruding the core 75 or 75', or for the foundation-forming

step, a neoprene core material is inserted into a die. As discussed above, the PVDF material is preferably introduced onto the core layer **75 (75')** such that a first outer layer **50** has a first polarity and a second outer layer **60** positioned contacting the core **75** opposing the first outer layer **50** has a second polarity, the second polarity being the reverse of the first polarity. Preferably, the fabrication process introduces the core material into the forming, cutting or extruding machine such that it terminates in the finished extruded product at a longitudinal distance away from the frame along the foundation layer (**100, Figure 6**). The frame pattern is then cut to form the foundation layer (which includes the core **75** and two opposing outer layers **50, 60** as discussed above). In a preferred embodiment, the foundation layer defines a linear arrangement of a plurality of sensor pads. An electrical signal path is positioned onto the external surface of the foundation layer **100**. Preferably, the electrical trace pattern is introduced onto the PVDF layer by applying a conductive ink in a silk screen pattern thereon. Preferably, a conductive electrical trace pattern is disposed onto two (preferably planar) separate surfaces of the two PVDF layers, the top outer surface and the bottom outer surface **50, 60**. The electrical pattern includes a sensor pad active region **220** and linear traces **221**. Further preferably, the same pattern is disposed as an external trace onto each transverse outer surface, such that the sensor array has two separate signal paths for each element **20**, the signal paths separated by the core material depth or thickness. Optionally, as noted above and illustrated by **Block 350**, the PVDF can be selectively polarized or selected portions of the outer layers can be de-polarized. For example, as schematically shown in **Figure 6A**, the frame portions which carry the linear external trace portions can be non-activated or heated to deactivate the PVDF material in that area to minimize the potential for signal excitation in this area so as to inhibit interaction or activation along the length of the array.

Figure 20A shows a preferred method of fabricating a low profile sensor having discrete elements as shown in **Figure 17A**. Generally described, a first unitary layer of PVDF film is configured with a laterally extending portion having a first width and a longitudinally extending portion having a second width. The longitudinally extending portion preferably extends from a lower edge of a center

of the lateral portion, thus forming a "T" shape configuration. Electrical traces are formed onto both major surfaces of the PVDF layer. The electrical traces are formed as a rectangular shaped sensor element onto the upper or lateral portion of the "T" such that this portion defines the two separate electrode regions with
5 opposing polarity. The electrical traces are formed onto the lower portion of the "T" to define three electrical paths. The first and second paths are formed on one major surface adjacent to one side to provide the electrical signal path for the first and second electrodes. The third path is formed on the opposite side of the PVDF layer (on the second major surface). The third path preferably includes a primary
10 finger portion. The third path forms the electrical ground and extends along the side of the second major surface opposite the side the first and second paths are formed on the first major surface.

A resilient core (such as neoprene) is inserted onto the top surface of one of the electrode regions. Linear strips of non-conducting film is positioned to overlay
15 the lower portion of the "T". A first electric shield material (such as MYLAR®) is positioned to overlay the lower portion of the "T" over the non-conducting (polyester) film on the side opposing the first major surface of the PVDF film (the side with the first and second electrical paths) and preferably includes a conductive finger portion. This conductive shield layer does not extend into the electrode
20 region. On the second outer surface, a "T" shaped conductive shield layer is configured and sized to mirror the PVDF film shape. This outer conductive shield layer is positioned to overlay the second major surface of the PVDF film in the electrode region and to overlay and contact the non-conducting film in the linear transmission layer.

25 The laterally extending portion of the PVDF film with the outer shield thereon is folded over the neoprene core such that the first and second electrode regions are positioned opposing the other with the core in contact with each and positioned intermediate thereof. The finger of the ground strip is folded up to contact the first conductive shield material thereby providing a substantially
30 continuous electric shield for the sensor while maintaining the electrical integrity of the electrode sensors. The transmission line is then preferably crimped at

predetermined portions to create the undulations along its length. The sensor is then preferably combined with a plurality of other sensors and packaged as a sensor array. The sensor array preferably includes a carrier member which is configured to hold the sensor elements in positional alignment until the sensor elements are secured to the patient. At that point, the carrier member can readily be detached from the individual sensor elements leaving them in place (in predetermined alignment) and structurally separate and physically isolated from the others. Stated differently, the sensor array is configured with a plurality of unitized sensors held by a unitizing member, and after applying the unitized array to a patient, the unitized member is readily removed leaving the sensors secured to a patient in a predetermined alignment.

Advantageously, the instant invention can provide a low profile sensor package which can be more responsive to acoustic signals measured on the external epidermal layer (conforms to patient chest area and flexes in response to chest movement). Further, the instant invention provides a smaller array package with closely positioned separately electrically activated sensor elements thereby allowing additional sensors in a smaller region to allow a more discerning sensor measurement. Further, the sensor array can selectively respond to the shorter wavelengths for the acoustic wave input of interest particularly those associated with evaluating coronary artery disease.

It will also be appreciated that the PVDF can be selectively activated in the sensor pad region as described above (or the PVDF be deactivated in the non-sensor pad region, preferably at least along the electrical traces) for all of the embodiments described herein.

It will also be appreciated that the sensor elements 20, 420 can be alternatively configured such as but not limited to a triangle, square, circle, parallelogram, octagon, and the like. Similarly, the discrete masses 900 or external stiffeners 910 can also be configured in alternative shapes such as but not limited to a triangle, square, circle, parallelogram, octagon, and the like.

While one embodiment of the present invention has been described with respect to a frame having two sides or rails, the present invention may also take the

form of a single frame or single rail member with sensors formed on one or both sides of the frame or rail or alternatively, discrete element sensors. Accordingly, the present invention should not be construed as limited to structures with a particular number of frame members or with a particular configuration of the frame but should encompass any frame structure or discrete sensor structure which allows for the differential operation of the sensor array according to the present invention.

The foregoing is illustrative of the present invention and is not to be construed as limiting thereof. Although a few exemplary embodiments of this invention have been described, those skilled in the art will readily appreciate that many modifications are possible in the exemplary embodiments without materially departing from the novel teachings and advantages of this invention. Accordingly, all such modifications are intended to be included within the scope of this invention as defined in the claims. In the claims, means-plus-function clauses are intended to cover the structures described herein as performing the recited function and not only structural equivalents but also equivalent structures. Therefore, it is to be understood that the foregoing is illustrative of the present invention and is not to be construed as limited to the specific embodiments disclosed, and that modifications to the disclosed embodiments, as well as other embodiments, are intended to be included within the scope of the appended claims. The invention is defined by the following claims, with equivalents of the claims to be included therein.

THAT WHICH IS CLAIMED IS:

1. A low profile acoustic sensor array, comprising:
a plurality of longitudinally extending sensor strips, each of said strips having at least one sensor element included thereon, wherein said at least one sensor element is configured so as to respond to acoustic wavelengths in the frequency range of interest and to inhibit response to compressional wavelengths in the frequency range of interest so as to mechanically filter acoustic signals detected by the sensor array.
2. A low profile acoustic sensor array according to Claim 1, wherein each of said plurality of longitudinally extending sensor strips comprise:
a plurality of longitudinally spaced apart separate sensor elements included thereon;
a sensor frame having a length and at least one longitudinally extending frame rail;
wherein each of said plurality of acoustic sensor elements attached to said at least one frame rail, wherein each of said acoustic sensor elements is sized and configured to extend transversely from said frame rail, and wherein each of said sensor elements have a pliable configuration; and
a plurality of separate electrical signal paths, at least one for each of said sensor elements, said electrical signal paths defining a signal path from a respective one of each of said sensor elements to a desired end electrical termination point.
3. An acoustic sensor array according to Claim 1, wherein each of said strips comprise a plurality of sensor elements, wherein said frame includes first and second transversely opposing frame rails, wherein said opposing rails are spatially separated along a major portion of said frame length, wherein each of said sensor elements is sized and configured to extend between said sensor frame opposing rails, and wherein each of said sensor elements is attached to a selected one of said

frame rails.

4. An acoustic sensor array according to Claim 2, wherein each of said strips is a unitary body along a major portion of its length, and wherein each of said sensor elements laterally extends from one of said at least one frame rails such that said sensor elements in each strip are linearly aligned along the length of said strip.

5. An acoustic sensor array according to Claim 3, wherein said sensor elements are arranged on said frame such that adjacent sensor elements are attached to different sides of said frame rails.

6. An acoustic sensor array according to Claim 2, said frame rails and said sensor elements have an upper surface, and wherein said upper surface of said frame rails and said sensor elements have a substantially constant and flat contour when viewed from the side when positioned on a subject.

7. An acoustic sensor array according to Claim 2, wherein said sensor array further comprises a plurality of discrete masses, one positioned on each of said sensor elements.

8. An acoustic sensor array according to Claim 6, said strip further comprising a longitudinally extending neck portion having opposing first and second ends, wherein said sensor element frame is attached to said neck portion first end and said termination point is an electrical connector positioned adjacent said neck second end.

9. An acoustic sensor array according to Claim 2, wherein each of said sensor elements comprises a first PVDF layer overlying and contacting a second flexible core layer and a third PVDF layer opposing said first layer and contacting said core layer.

10. An acoustic sensor array according to Claim 9, wherein said electrical signal paths are formed by a conductive pattern formed onto said first and second PVDF film layers.

11. An acoustic array according to Claim 8, wherein said frame rails comprise a first PVDF layer, a second intermediate core layer, and a third PVDF layer, wherein said first and third PVDF layers sandwich said second core layer.

12. An acoustic array according to Claim 10, wherein said frame rails and said sensor elements comprise the same multi-layer materials in the same thicknesses.

13. An acoustic array according to Claim 9, wherein said first layer PVDF is selectively actively polarized about portions of sensor elements and substantially non-actively polarized about said frame sides to provide increased signal isolation.

14. An acoustic array according to Claim 2, wherein said plurality of strip arrays is four.

15. An acoustic array according to Claim 13, wherein said plurality of sensor elements is six.

16. An acoustic array according to Claim 9, wherein said core layer comprises neoprene.

17. An acoustic array according to Claim 11, wherein said electrical signal path is defined by two spatially separate opposing electrical traces formed onto said first and third PVDF layers, said separate electrical traces including a first electrical linear trace with a first rectangular sensor element region and a corresponding second linear trace with a second rectangular sensor element region, wherein said first electrical linear trace and first rectangular region disposed onto

said first PVDF layer and said second electrical linear trace and second rectangular region disposed onto said third PVDF layers.

18. An acoustic sensor element suitable for use in said array of Claim 1, said sensor element comprising:

a resilient core layer comprising a low permittivity material having a core thickness;

5 a first pliable material layer overlaying and contacting said core layer, said first material layer comprising a piezoelectrically active material, said first pliable layer having opposing internal and external surfaces;

a second pliable material layer overlaying and contacting said core layer opposing said first pliable material layer, said second pliable layer comprising a
10 piezoelectrically active material and having opposing internal and external surfaces;

a first electrical trace disposed on said first pliable material layer inner surface; and

a second electrical trace disposed on said second pliable material layer
15 inner surface such that said first and second electrical traces face each other across said core layer, wherein during operation and in response to flexure of said sensor element, said first and second electrical traces generate respective first and second voltages, and wherein said first and second voltages have opposing polarity.

19. An acoustic sensor according to Claim 18, wherein said core layer comprises neoprene.

20. An acoustic sensor according to Claim 18, wherein said core thickness defines the separation distance between said first and second pliable layers.

21. An acoustic sensor according to Claim 20, wherein said first and second pliable material layers are formed from PVDF.

22. An acoustic sensor according to Claim 19, wherein said core layer has a first relative permittivity and said first and second pliable material layers have a second relative permittivity, such that said first relative permittivity is at less than said second relative permittivity.

23. An acoustic sensor according to Claim 21, wherein said core layer has a thickness of about 30 microns, and wherein said first and second pliable layers have a thickness of about 600 microns.

24. An acoustic sensor according to Claim 17, wherein said operational frequency range includes at least the frequency range of about 100 to 1000 hertz.

25. An acoustic sensor according to Claim 24, wherein said sensor generates a response during flexure which has an output substantially equal to the voltage differential between said first and second voltages.

26. An acoustic strip sensor array, comprising:
a sensor frame having a frame length and including at least one longitudinally extending rail;

a plurality of acoustic sensor elements attached to said rail, wherein said acoustic sensor element is sized and configured to extend a transverse distance away from said rail, said sensor element having a pliable configuration; and

first and second opposing spatially separate electrical signal paths for each of said sensor elements, wherein in response to flexure of said sensor elements, said first and second electrical signal paths are configured to provide opposing polarities defining a differential signal output for a respective one of each of said sensor elements.

27. An acoustic strip sensor array according to Claim 26, wherein said acoustic strip sensor array has a substantially planar profile along said frame and said sensor elements when viewed from the side.

28. An acoustic strip sensor array according to Claim 26, wherein said frame and said sensor elements are sized and configured to flex in response to movement associated with shear waves and to inhibit element flexure associated with long compression waves in the acoustic frequency range of interest.

29. An acoustic strip sensor array according to Claim 26, wherein when engaged on the surface of a patient, said sensor elements flex in response to acoustic waves having a propagation velocity of less than about 100m/s, and wherein said sensor elements are sized and configured to inhibit flexure in response to acoustic waves having a propagation velocity longer than about 300 m/s.

30. An acoustic strip sensor array according to Claim 26, wherein said sensor elements and said frame elements comprise a resilient core layer and opposing first and second outer layers comprise PDVF.

31. An acoustic strip sensor array according to Claim 30, wherein said first and second electrical signal paths are positioned to be on internal surfaces of said first and second outer layers, positioned with respect so said core to face the other across the width of said core, such that, during operation and engagement with a patient, flexure of said sensor generates a first and second response voltage corresponding to a respective one of said first and second electrical signal paths, wherein said sensor array signal output for each sensor element is defined by the voltage differential between said first and second voltages.

32. An acoustic strip sensor array according to Claim 31, further comprising a plurality of discrete masses, at least one each attached to each of said plurality of acoustic sensor elements.

33. An acoustic strip sensor array according to Claim 30, wherein said core layer has a first relative permittivity and said first and second pliable material layers have a second relative permittivity such that said first relative permittivity is

less than said second relative permittivity.

34. An acoustic strip sensor array according to Claim 25, wherein said sensor array has an operational frequency range which includes the frequency range of about 100 to 1000 hertz.

35. An acoustic strip sensor array according to Claim 30, wherein said strip sensor array is configured such that said first and second electrical signal paths are defined by traces formed on the internal facing surfaces of said first and second outer layers, and wherein said signal paths include a ground plane defined
5 by an electrical trace formed on the externally facing surfaces of said first and second outer layers.

36. An acoustic strip sensor array according to Claim 26, wherein said frame and said acoustic sensor elements define a unitary body.

37. A method for fabricating the strip sensor array of Claim 1, comprising the steps of:

forming a unitary body strip sensor foundation layer having opposing major surfaces;

5 forming a series of proximately positioned non-contacting pads and a frame segment into the foundation layer;

positioning two separate opposing PVDF layers on opposing major surfaces of the foundation layer, the PVDF layers including two major surfaces and an electrical signal path formed on one surface and a ground path formed on the other;

10 and

orienting the PVDF layers such that the electrical signal paths of each of the PVDF layers faces the foundation layer.

38. A method according to Claim 37, wherein said second forming step further comprises forming the frame segment to include two longitudinally extending opposing sides, and arranging the series of pads on the foundation layer

- to attach to at least one of the two opposing sides and to transversely extend
- 5 between the two sides.

39. A method according to Claim 38, wherein said positioning step is performed by disposing a series of electrically separate external traces onto a first major surface of the PVDF layers, the electrical traces including a linear extending signal path and an electrode region corresponding to the sensor element pads.

40. A method according to Claim 39, further comprising the step of disposing a series of discrete masses onto an exposed surface of one of the PVDF layers.

41. A method according to Claim 37, wherein the PVDF layers are configured to provide output voltages of opposing polarities in response to a flexure input.

42. A method according to Claim 37, wherein predetermined portions of the longitudinally extending sides are selectively polarized.

43. A method according to Claim 37, wherein said PVDF layer electrical traces are formed by disposing a conductive layer in a predetermined conductive pattern thereon.

44. A method of detecting acoustic wave signals to identify the condition of a patient's coronary arteries, using the sensor array of Claim 1, comprising the steps of:

- positioning a sensor array having a plurality of pliable sensor elements and
- 5 first and second opposing piezoelectrically active layers positioned over a center neutral core onto a patient's exposed surface in a chest region of interest;
- securing each of said plurality of sensor elements to the patient such that they are conformal to the surface of a patient;
- flexurally displacing at least one sensor element in response to a detected

- 10 shear wave in an acoustic frequency of interest, the flexural displacement generating a first voltage having a first polarity associated with said first piezoelectric active layer and a second voltage having an opposing polarity associated with said second piezoelectric active layer; and
- combining the first and second voltages to generate an output signal for the
- 15 flexed sensor responsive to the change in curvature of the patient surface associated with the detected shear wave.

45. An acoustic sensor array, comprising:
- a plurality of unitary acoustic sensor elements;
- a plurality of transmission lines having opposing first and second ends and defining a length therebetween, a respective one transmission line for each of said
- 5 plurality of unitary acoustic sensors, said transmission line first end individually attached to a respective one of said acoustic sensor elements; and
- wherein each of said transmission lines is configured with a series of undulations along its length.

46. An acoustic sensor array according to Claim 45, wherein said array is configured such that each of said unitary sensor elements are structurally separate and discrete from the others along the sensor element and transmission line.

47. An acoustic sensor array according to Claim 46, wherein said undulations are formed onto said transmission lines as a series of continuously repeating pleated segments.

48. An acoustic sensor array according to Claim 45, wherein said plurality of elements comprises three linearly arranged substantially flat elements.

49. An acoustic sensor array according to Claim 46, further comprising a connector configured to receive a portion of each of said transmission line second ends therein.

50. An acoustic sensor array according to Claim 46, wherein said sensor element includes a piezoelectrically active film configured to define two spatially separated opposing electrode surfaces with opposing polarities, and wherein during operation said opposing electrode surfaces produce first and second voltages, respectively, and each of said sensor elements is configured to generate a signal output defined by the voltage differential between said first and second voltages in response to flexure of said electrode surfaces.

51. An acoustic array according to Claim 45, further comprising a carrier member releasably attached to each of said sensor elements.

52. An acoustic array according to Claim 45, further comprising a plurality of discrete masses, at least one attached to each of said plurality of sensors.

53. An acoustic array according to Claim 52, wherein said discrete mass includes a reflective surface thereon.

54. A sensor array according to Claim 45, wherein said sensor element comprises:

a resilient core layer comprising a low permittivity material having a core thickness;

5 a first pliable material layer sized and configured to sandwich and overlay said core layer, said first material layer comprising a piezoelectrically active material having opposing first and second major surfaces;

10 first and second electrical traces disposed on said first major surface of said first pliable material layer, said first and second electrical traces defining a spatially separate first and second electrode, wherein in position over said core, said first electrode has an opposite polarity relative to said second electrode; and

an exterior conductive shield layer sized and configured to overlay

15 said second major surface of said first material layer;
and wherein said transmission line defines a linear transmission line attached to
said sensor element, said linear transmission line including first and second ends
and extending a linear length therebetween, comprising;

20 a first pliable material layer extending from said first end to said
second end of said linear transmission line having opposing first and
second major surfaces, said first pliable material layer comprising a
piezoelectrically active material;

25 first, second, and third electrical traces disposed on said first pliable
material layer in electrical communication with said sensor element first
material layer electrical traces, said first and second electrical traces
disposed on said first major surface and said third electrical trace disposed
on said second major surface;

30 first and second layers of a non-conducting film configured and
sized to respectively overlay a major portion of said first and second major
surfaces of said first pliable material layer;

 a first linear outer layer conductive strip configured and sized to
overlay a major portion of first non-conducting film layer opposite said first
major surface of said first pliable material layer; and

35 a second linear outer layer conductive strip configured and sized to
overlay a major portion of said second non-conducting film layer opposite
said second major surface of said first pliable material layer;

40 wherein said first pliable material layer of said transmission line and
said first pliable material layer of said sensor element is a unitary layer, and
wherein said third electrical trace of said first pliable material layer
provides an electrical ground operably associated with said first and second
conductive outer layers of said sensor.

55. An acoustic sensor according to Claim 54, wherein said
transmission line is configured with a series of undulations along its length.

56. An acoustic sensor according to Claim 54, further comprising at

least one discrete mass attached to said sensor element.

57. An acoustic sensor array, comprising:
a plurality of compliant sensor elements having first and second
outer surfaces, said first outer surface configured to attach to a subject such
that it is substantially conformal to the subject; and
5 a carrier member releasably attached to said second outer surface of
each of said plurality of sensor elements to hold said plurality of sensors in
alignment during positioning on a subject;
wherein said carrier member is disengaged from said sensor
elements after said sensor elements are attached to a desired location on the
10 subject without causing said sensor elements to move from the desired
location.

58. An acoustic sensor array according to Claim 57, wherein said carrier
member includes an externally accessible tab.

59. An acoustic sensor array according to Claim 57, further comprising
a plurality of discrete masses, at least one attached to each of said sensor elements.

60. An acoustic sensor array according to Claim 59, wherein a
predetermined number of said discrete masses includes a reflective surface.

61. An acoustic sensor array according to Claim 57, further comprising
a plurality of discrete stiffeners, at least one attached to each of said sensor
elements.

62. An acoustic sensor array according to Claim 61, wherein a
predetermined number of said stiffeners includes a reflective surface.

63. An acoustic sensor array according to Claim 57, further comprising
a plurality of transmission lines and a connector, wherein each of said sensor

elements are operably associated with a respective one of said transmission lines, and wherein each of said transmission lines are connected to said connector.

5

64. An acoustic sensor array according to Claim 63, wherein each of said transmission lines are configured with a series of undulations along its length.

65. An acoustic sensor array according to Claim 57, said wherein said sensor elements comprise opposing first and second electrodes having opposing polarities and a center core having a thickness disposed therebetween, wherein said electrodes are defined by a piezoelectrically active film and wherein said core
5 thickness defines the separation distance between said first and second electrodes.

66. A method of forming an acoustic sensor for an acoustic array of Claim 45, said acoustic sensor having a sensor pad region and a transmission line, comprising the steps of:

5 configuring a first unitary layer of PVDF film having first and second opposing major surfaces with a laterally extending region having a first width and a longitudinally extending region having a second width;

forming sensor element electrical traces onto the first major surfaces of the PVDF layer, the sensor electrical traces are arranged as a rectangular shape onto
10 the lateral region of the PVDF layer such that the lateral region defines first and second separate electrode regions with opposing polarity;

forming electrical traces onto the longitudinally extending region of the first and second major surfaces of the PVDF layer to define three electrical paths, wherein the first and second paths are formed on one major surface to provide the
15 electrical signal path for the first and second electrode regions, and wherein the third path is formed on the opposing major surface of the PVDF layer and is configured with a primary finger portion;

inserting a resilient core onto a surface of one of the electrode regions;

positioning non-conducting film to overlay substantially the entire length of
20 the longitudinally extending region of the PVDF layer;

positioning a first electric shield material to overlay the non-conducting

film on the side opposing the first major surface of the PVDF film, wherein the first electrical shield includes a conductive secondary finger portion;

providing a second electric shield layer configured and sized to mirror the
25 PVDF film shape, to overlay the second major surface of the PVDF film in the laterally extending electrode region and to overlay and contact the non-conducting film in the longitudinally extending region;

folding the laterally extending region of the PVDF film over the core such that the first and second electrode regions are positioned opposing the other with
30 the core is positioned intermediate thereof; and

folding the primary finger of the ground strip to overlay the first major surface, wherein electrical contact between the first and second conductive shield material at the termination end thereby provides a substantially continuous electric shield for the sensor.

67. A method according to Claim 66, further comprising the step of forming undulations along a portion of the length of said longitudinally extending region.

68. A method of minimizing the mechanical or electrical interference between one or more of adjacent sensors or undesired system or environmental mechanical input in a flexure responsive acoustic sensor array having a plurality of
5 sensor elements and a plurality of transmission paths, comprising the step of forming a series of undulations in the transmission paths operably associated with the sensor elements to provide mechanical damping therealong.

69. A method according to Claim 68, wherein the acoustic sensor array comprises a plurality of sensor elements and a separate electrical transmission path for each of said sensor elements, said method further comprising the step of
5 forming the sensor array such that the plurality of sensor elements and associated sensor electrical transmission paths are physically separate units.

70. A method of arranging the sensor array of Claims 1 and 45 on a

subject, wherein said sensor array has a plurality of discrete sensor elements associated therewith and a unitized carrier member holding same in predetermined alignment onto a patient, comprising the steps of:

- 5 arranging the discrete sensor elements of the array onto the patient while the carrier member holds the sensor elements in predetermined alignment;
- securing the sensor elements to the skin of the subject in a desired location; -
- and
- subsequently removing the carrier member by peeling same away from the
- 10 top surface of the sensor elements, leaving the sensor elements in alignment on the patient.

71. A method according to Claim 70, wherein said sensor array includes a plurality of transmission lines, one attached to each of said sensor elements, and wherein said transmission lines are configured with a series of undulations thereon.

72. A method according to Claim 70, wherein each of said sensor elements include at least one discrete mass positioned on an outer surface thereof such that it is attached to said sensor element and in contact with said unitized carrier member prior to the mechanical separation.

73. A method according to Claim 72, wherein a predetermined number of said discrete masses includes a reflective surface thereon.

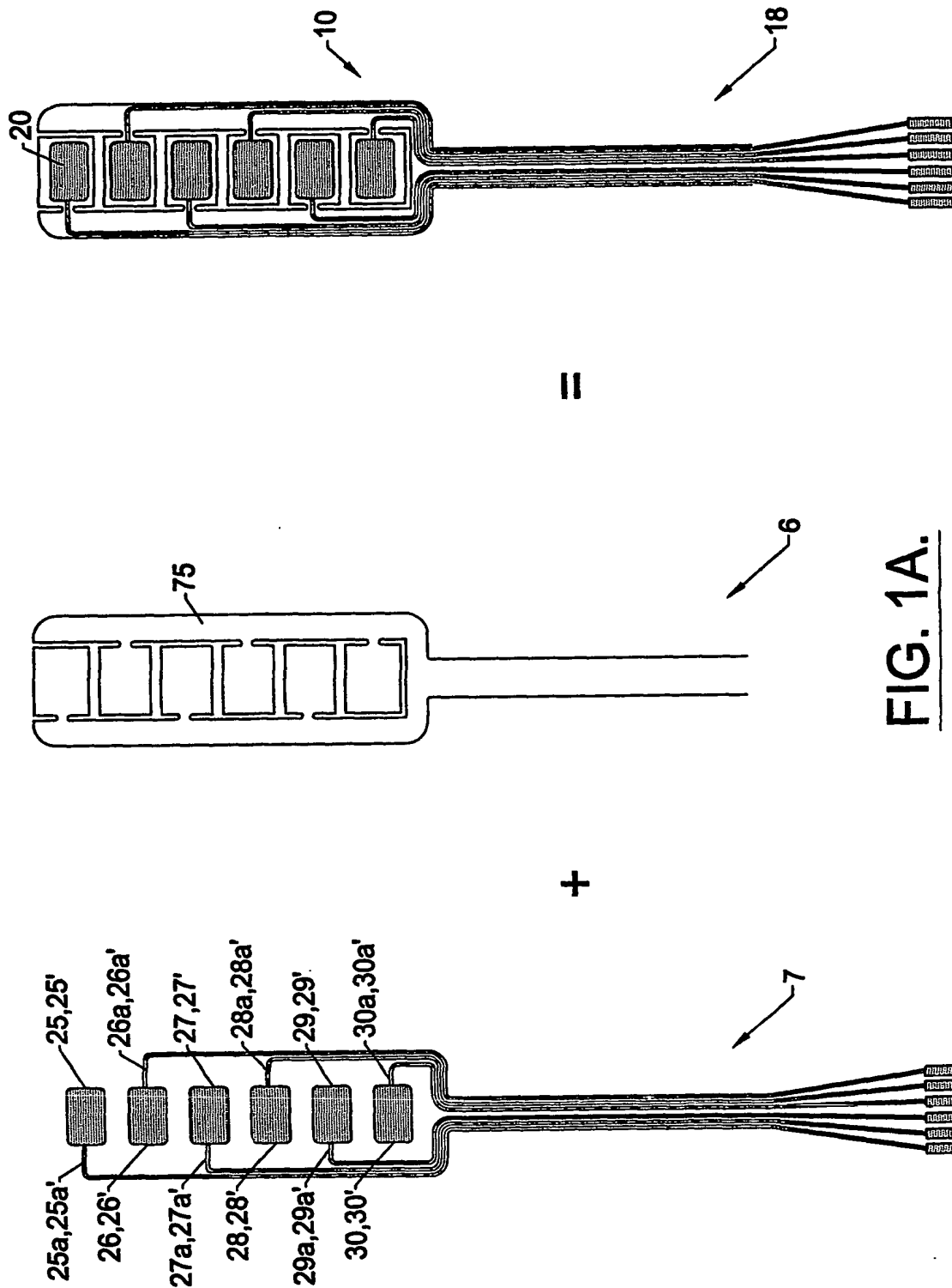
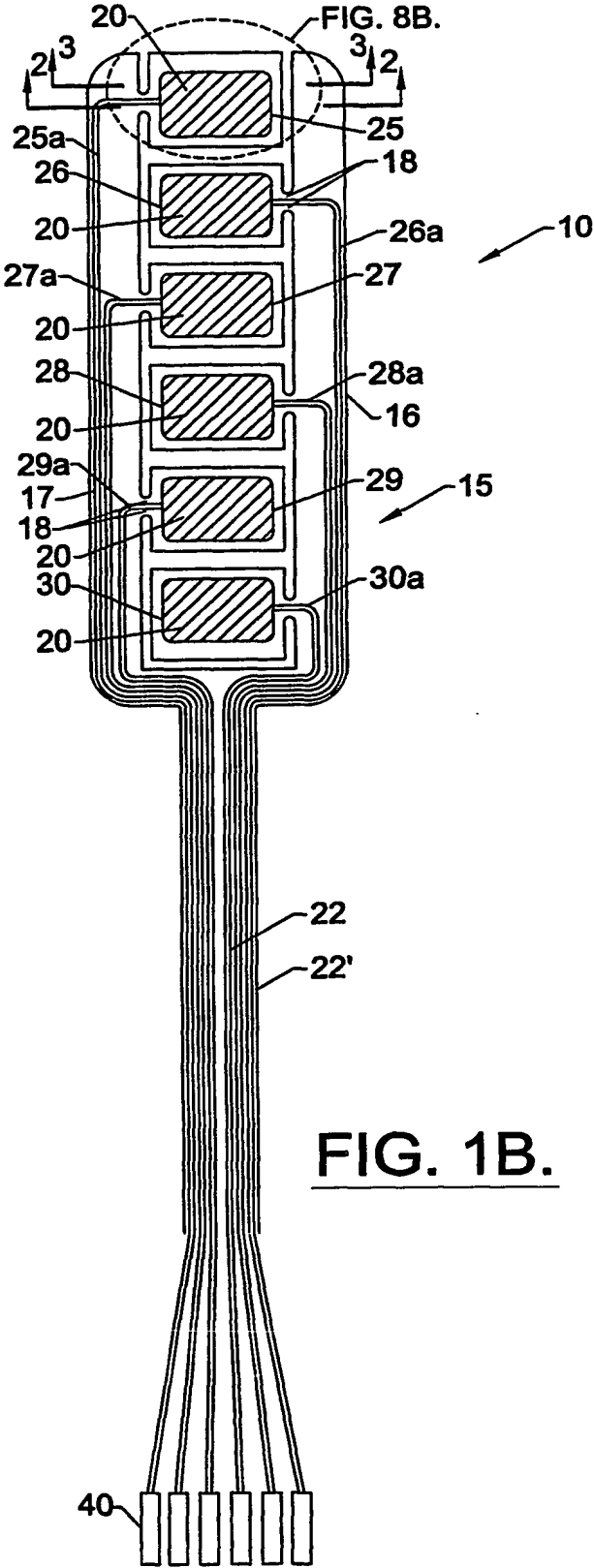


FIG. 1A.



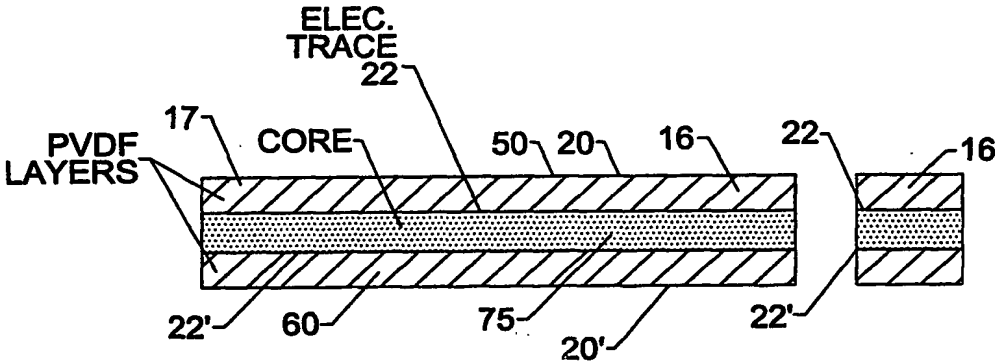


FIG. 2.

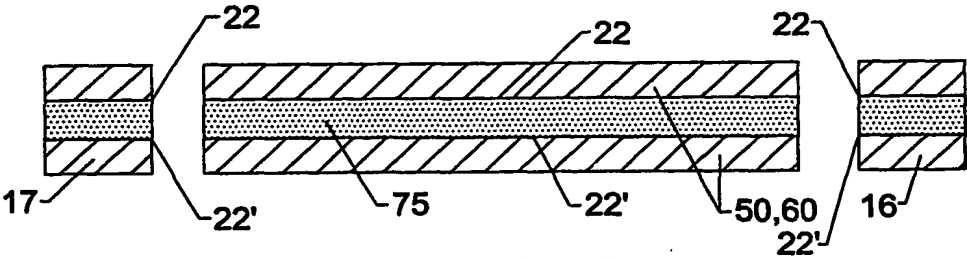
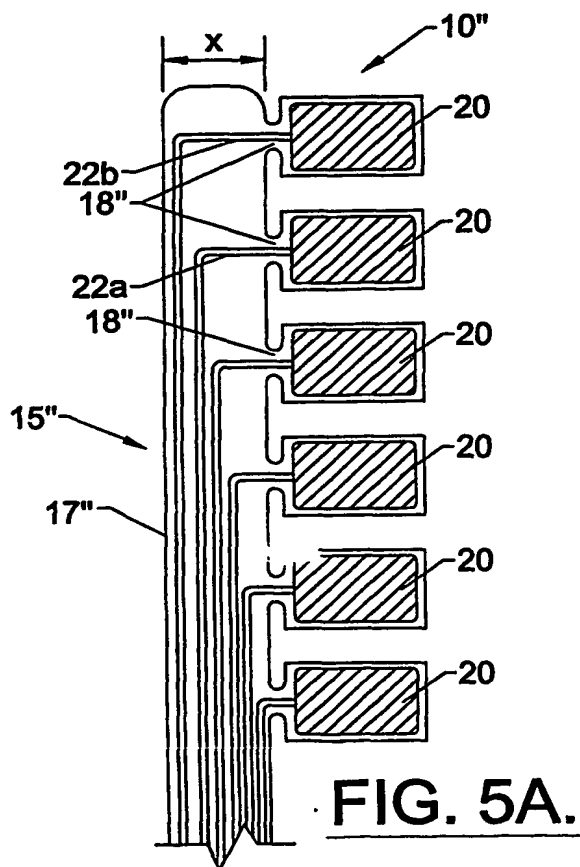
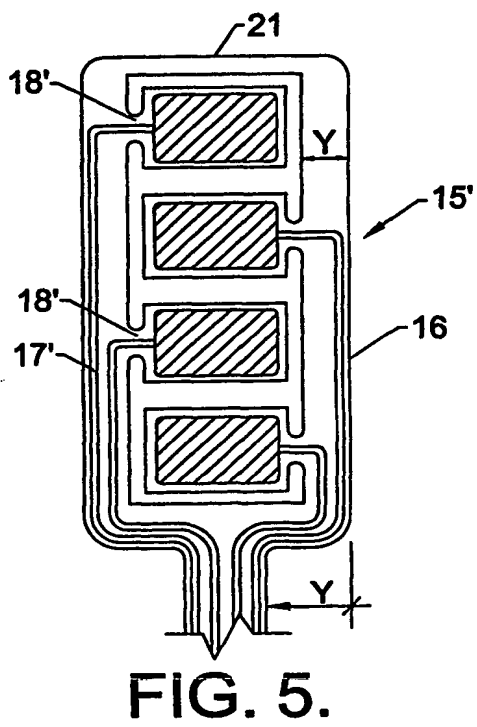
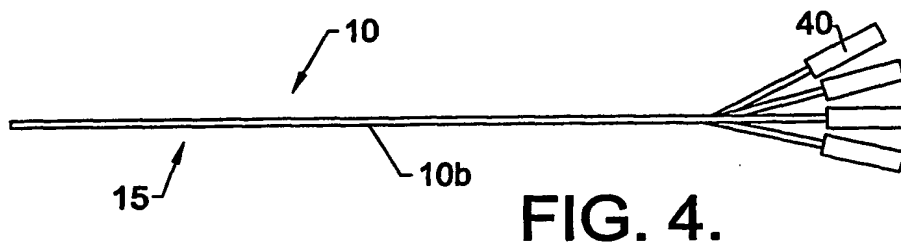


FIG. 3.



5/30

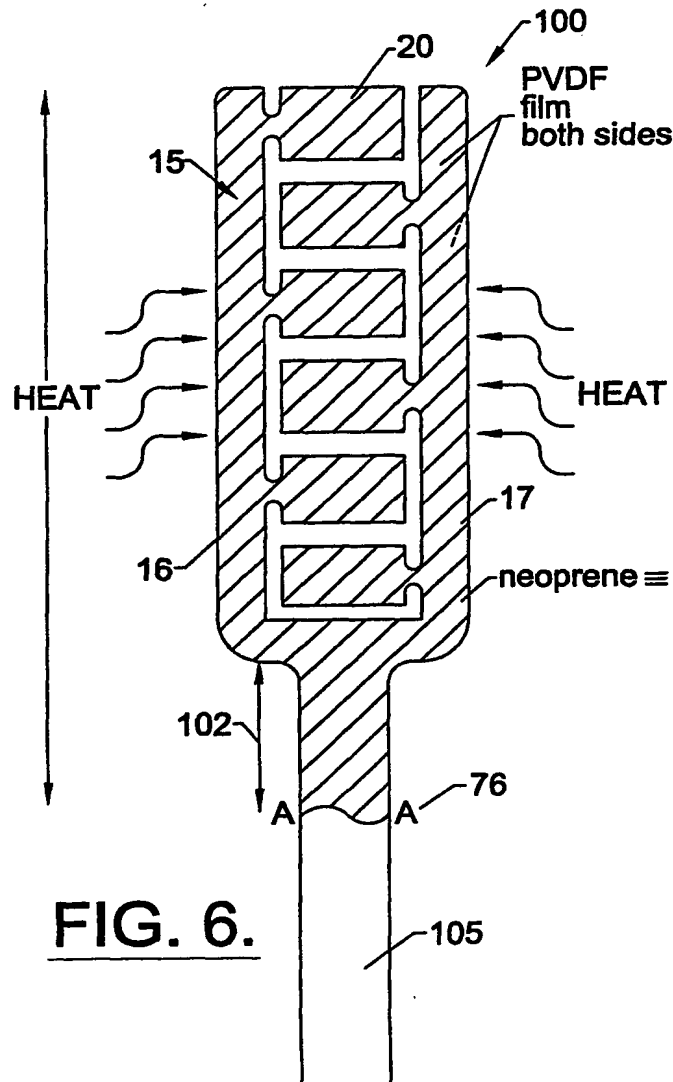


FIG. 6.

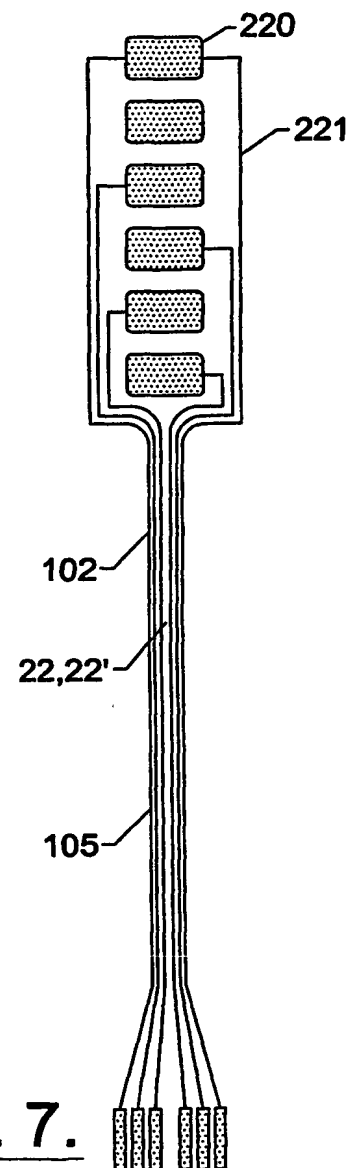
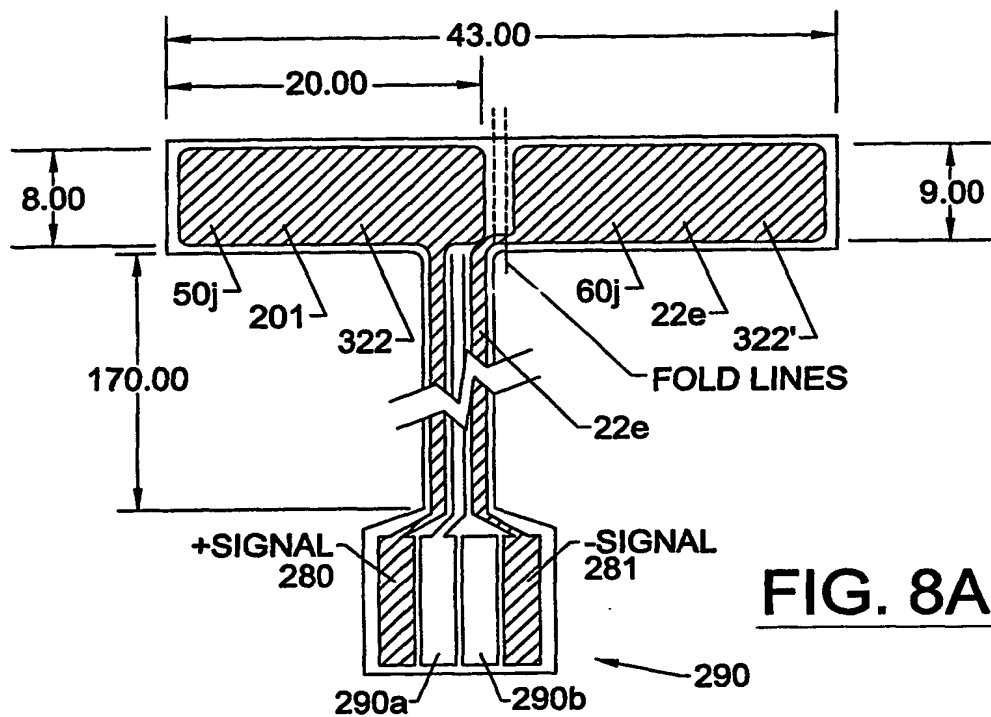
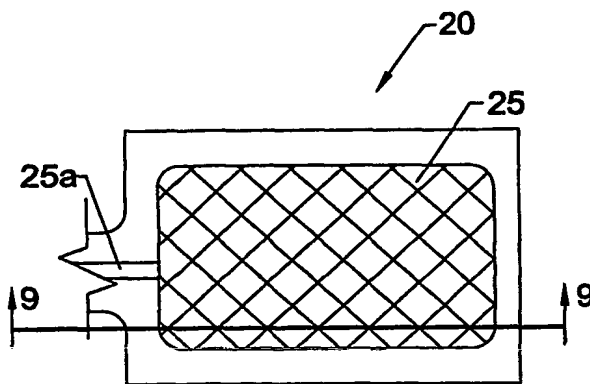
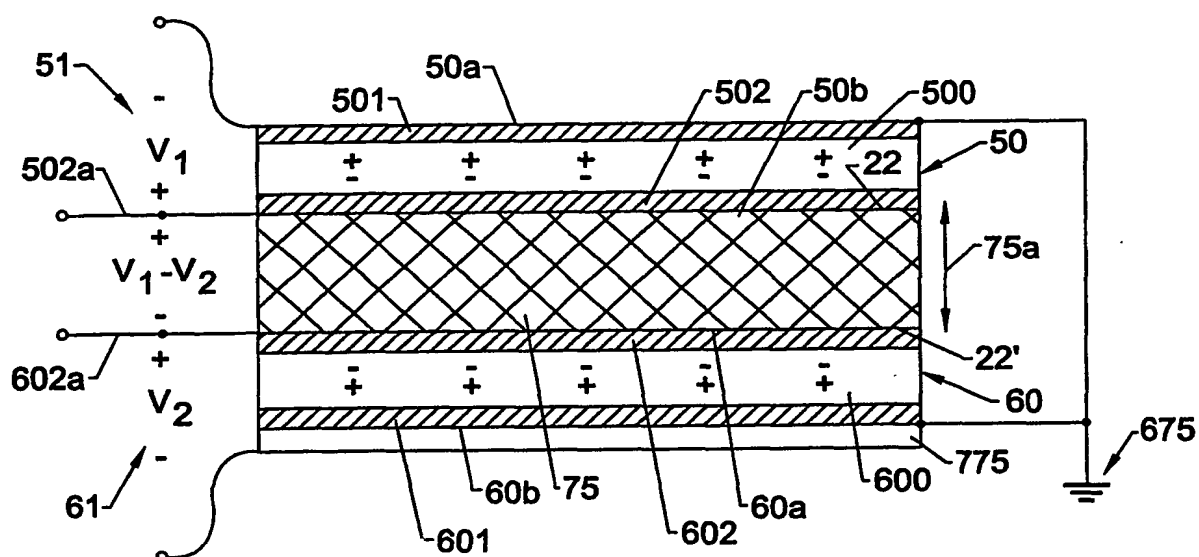


FIG. 7.

6/30

FIG. 8A.FIG. 8B.

7/30

**FIG. 9.**

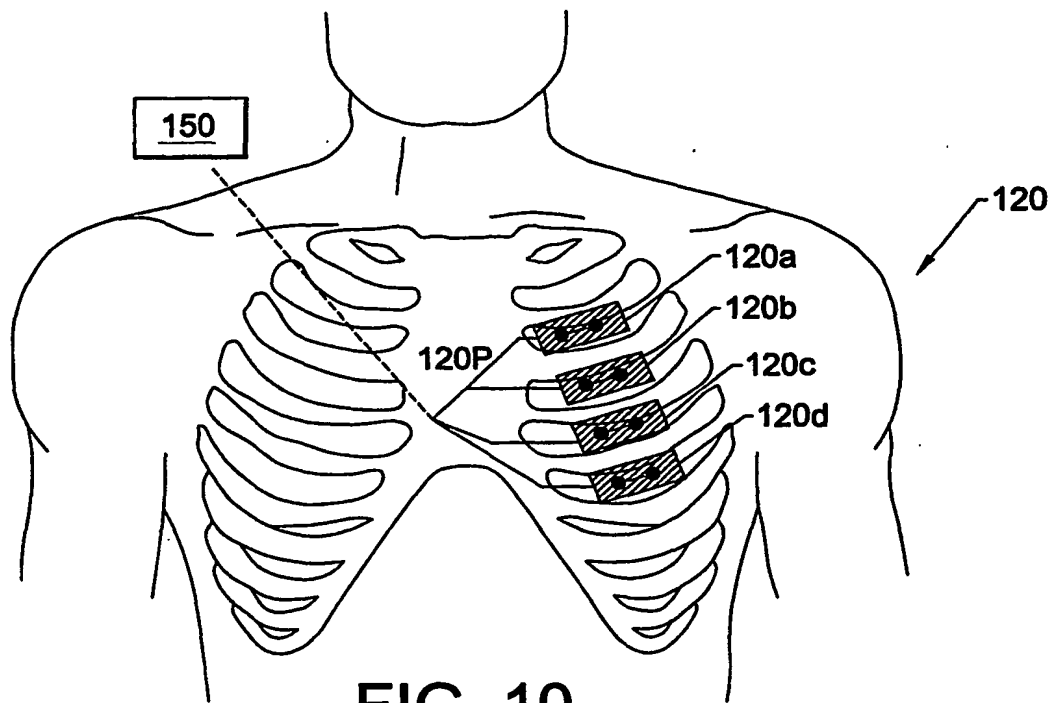
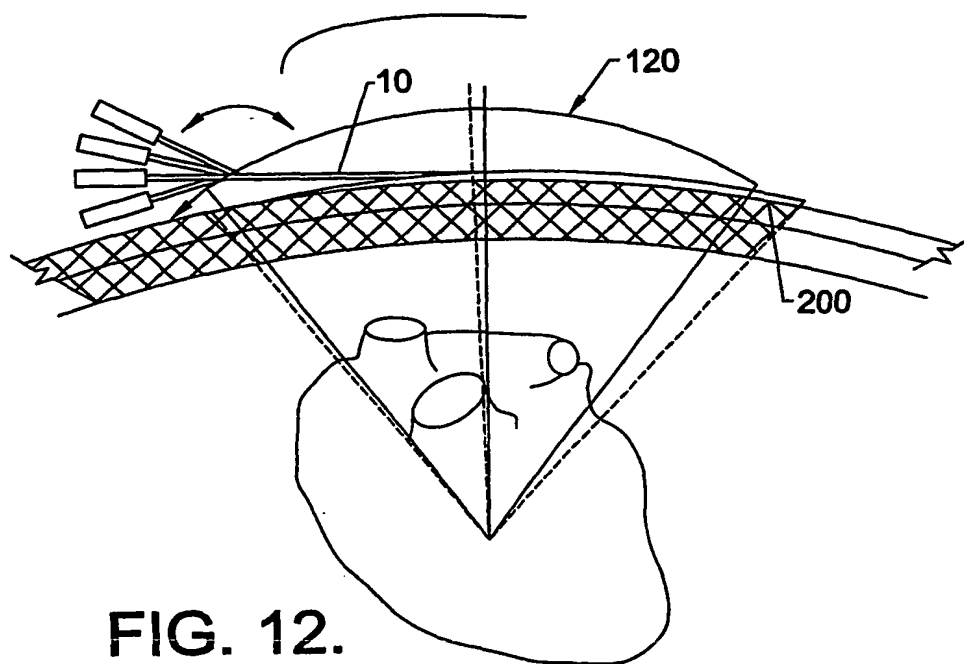
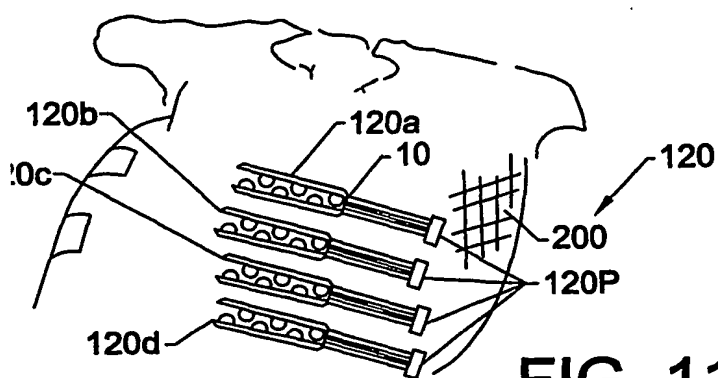
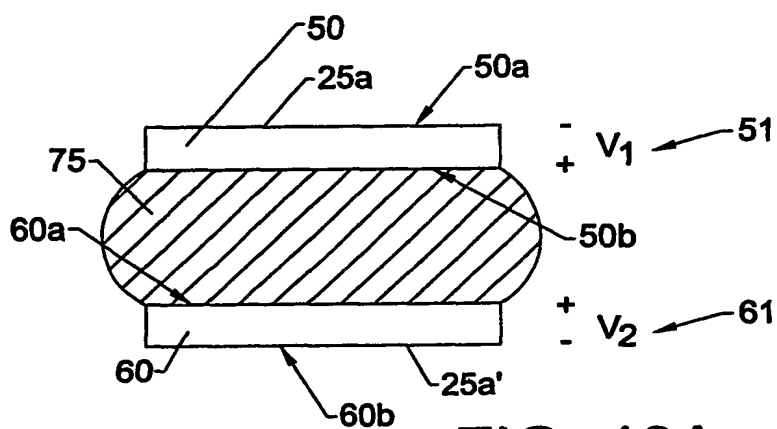
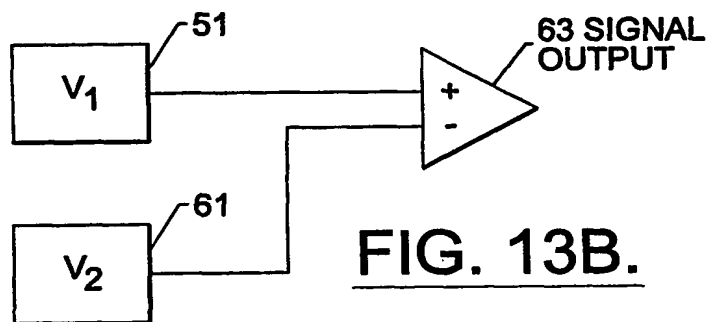


FIG. 10.

9/30



10/30

FIG. 13A.FIG. 13B.

11/30

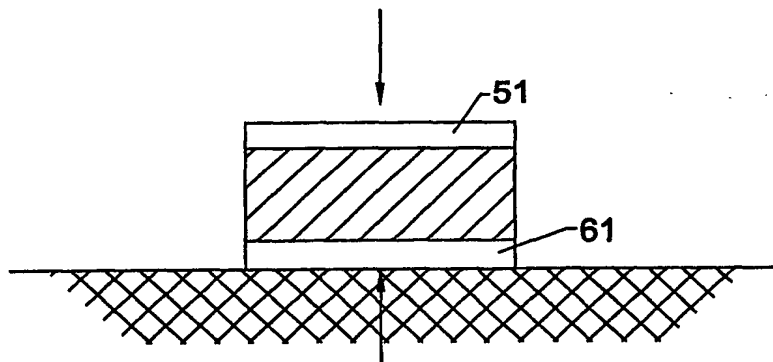


FIG. 14A.

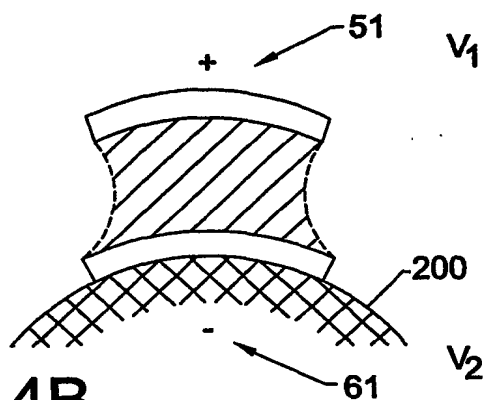


FIG. 14B.

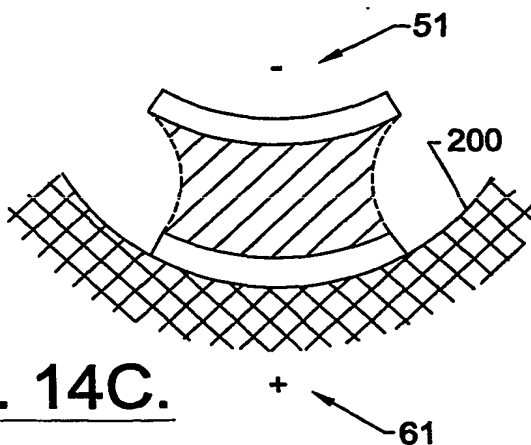


FIG. 14C.

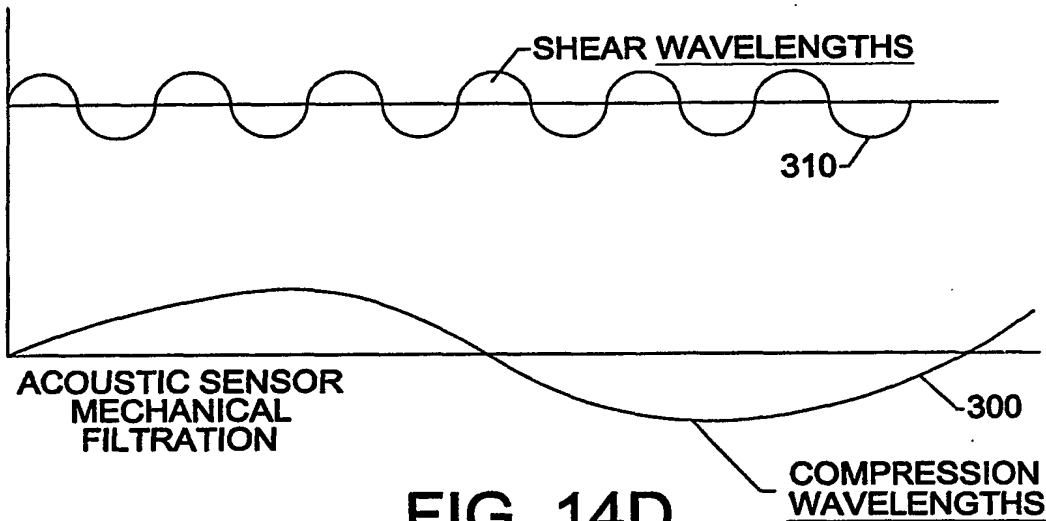


FIG. 14D.

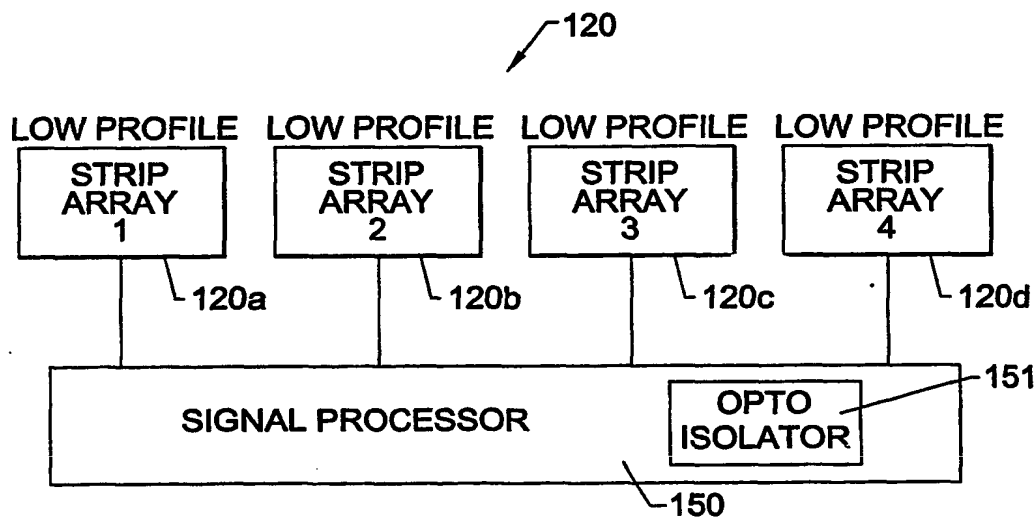
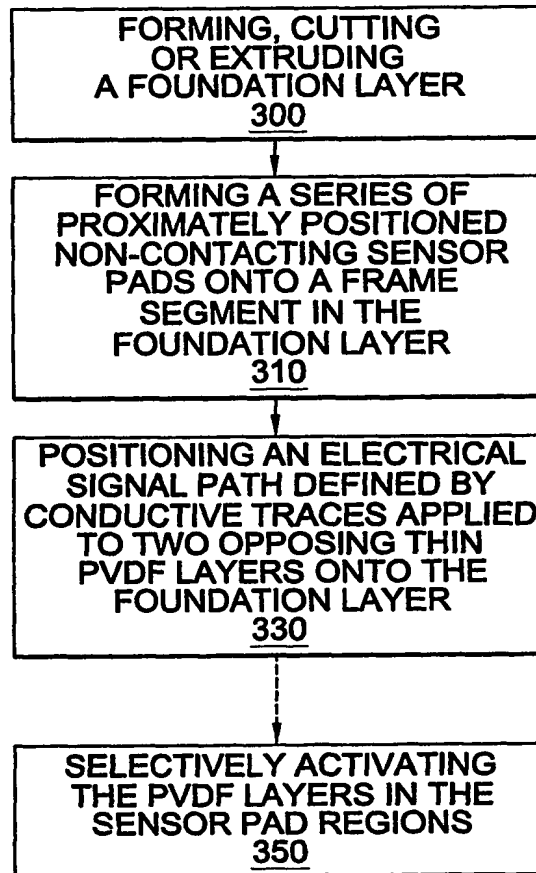
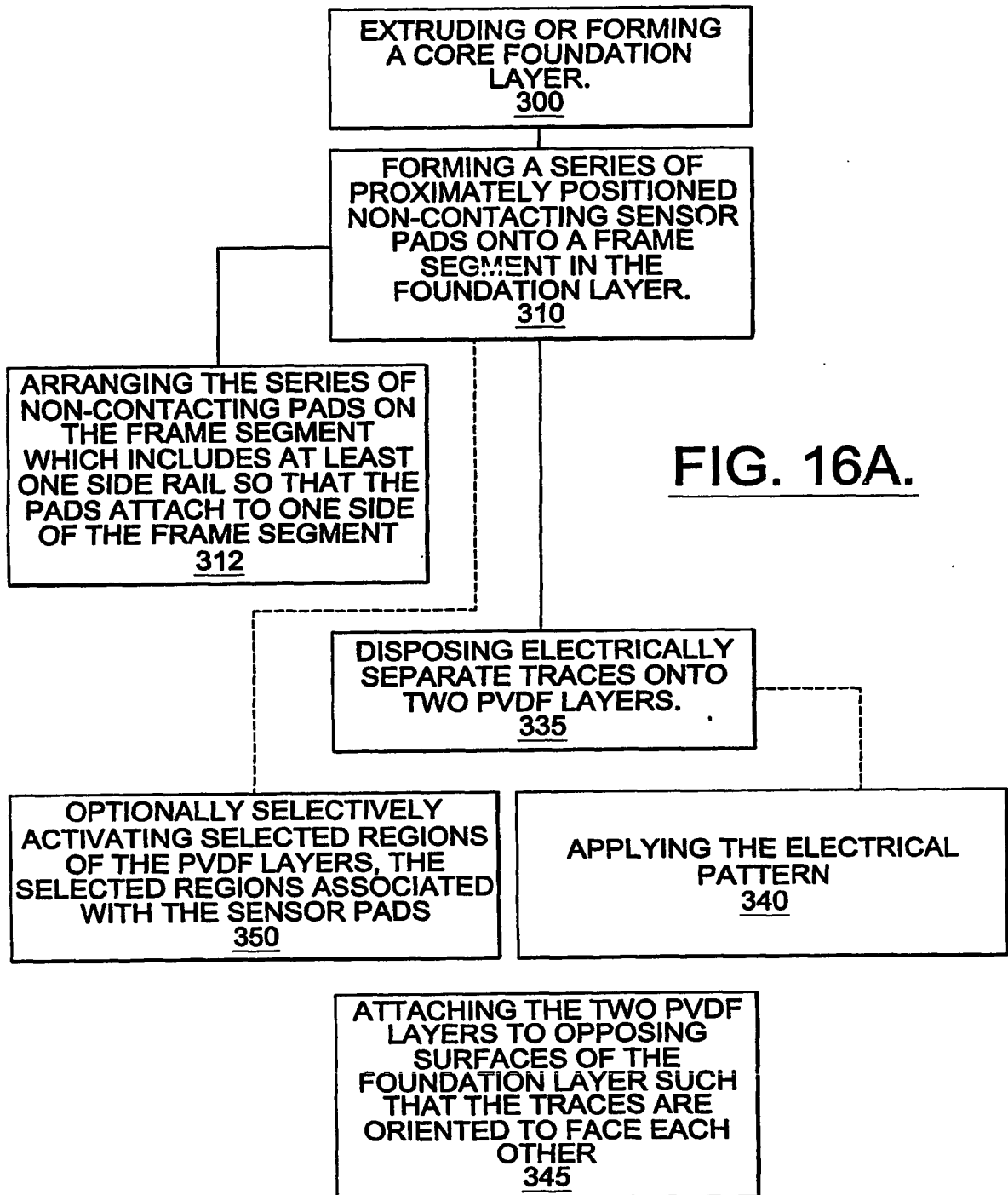


FIG. 15.

13/30

FIG. 16.

14/30



15/30

TO SIGNAL
PROCESSOR

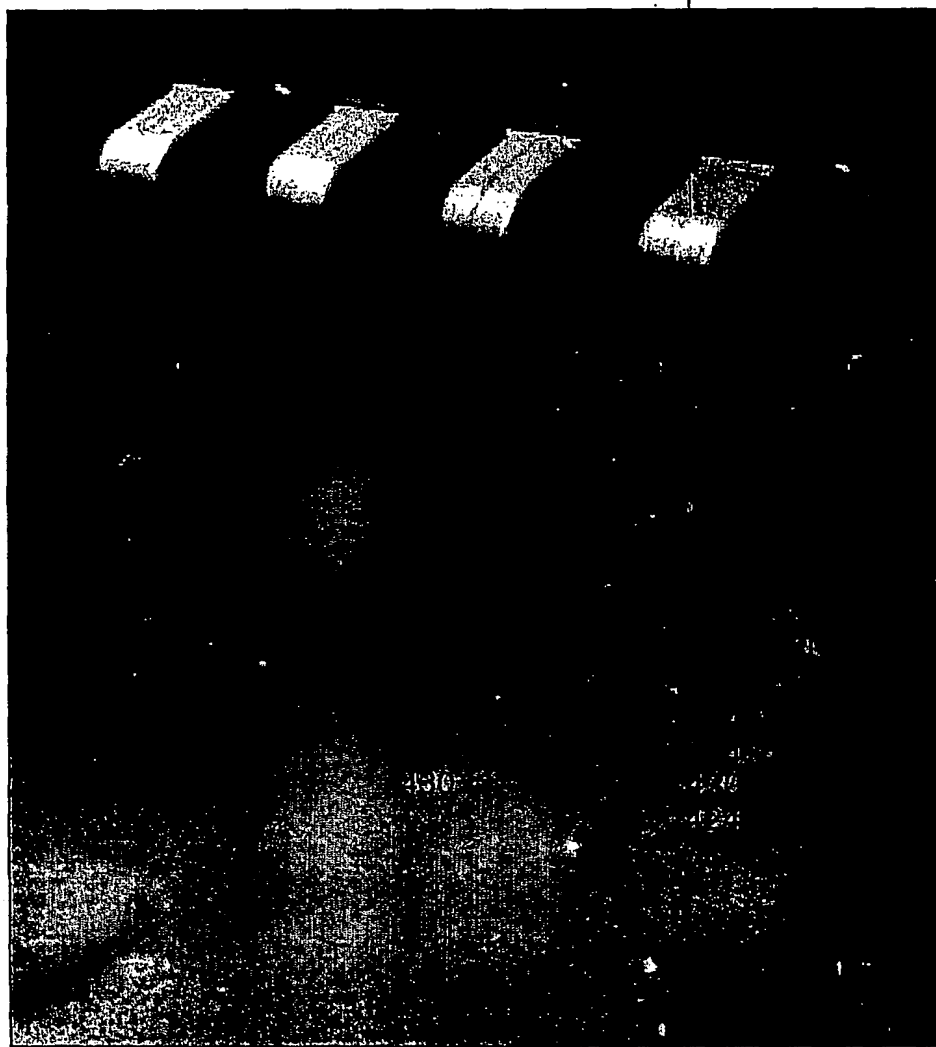


FIG. 17A.

16/30

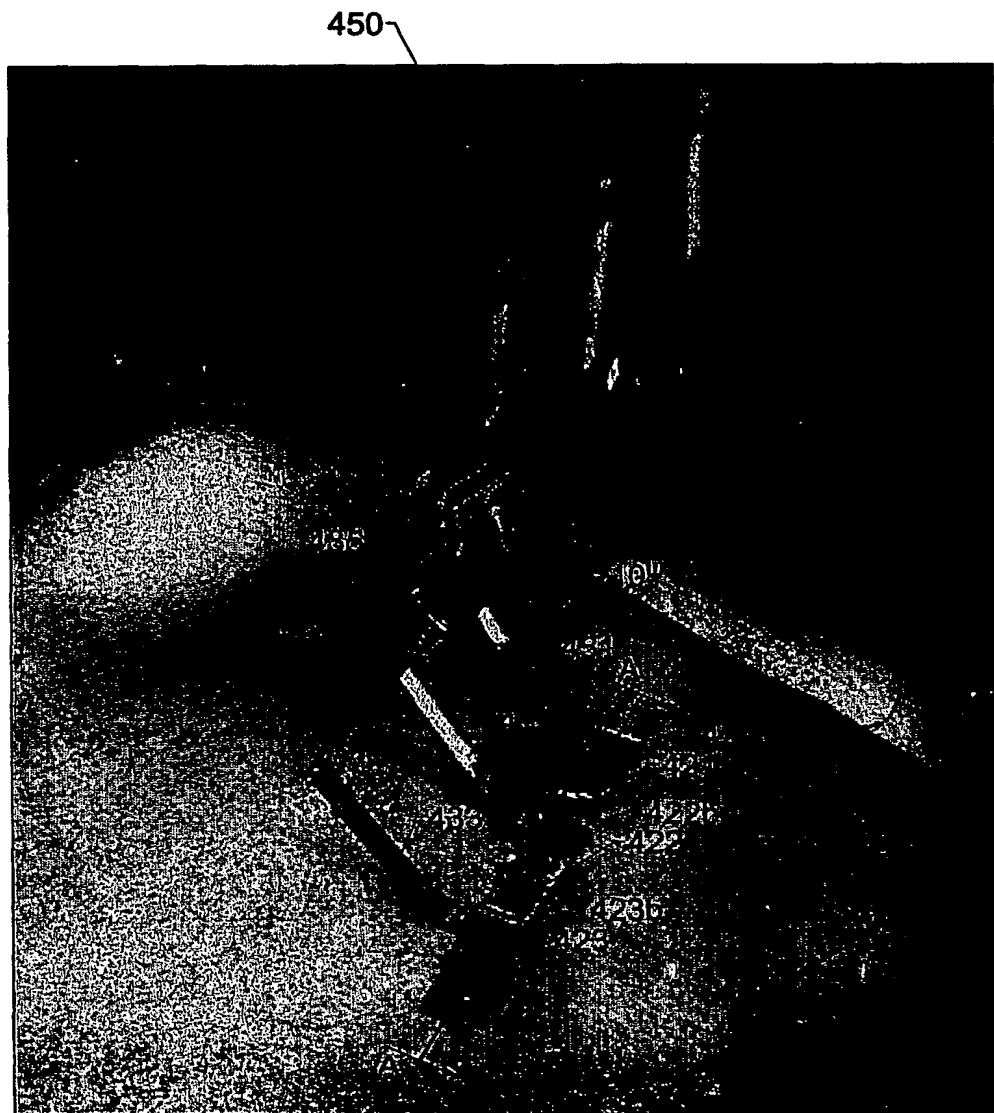


FIG. 17B.

17/20

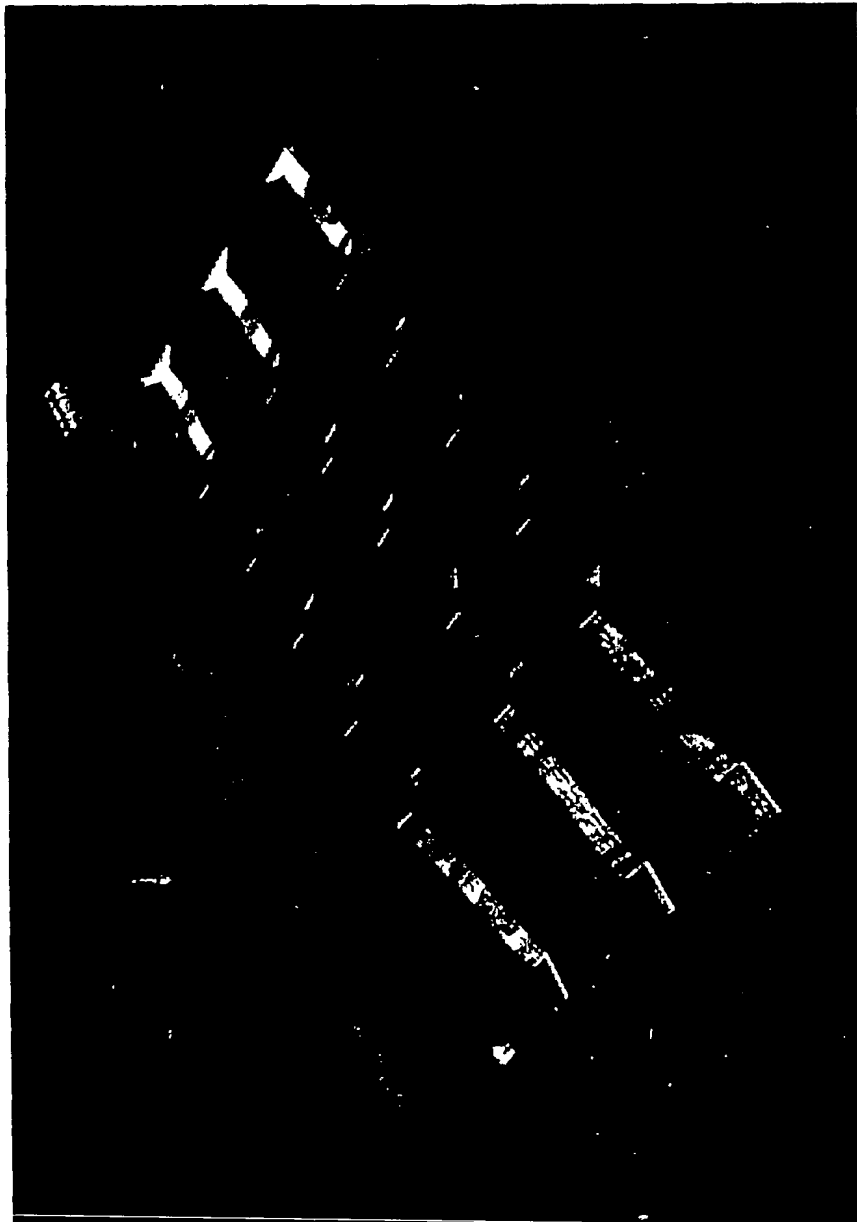
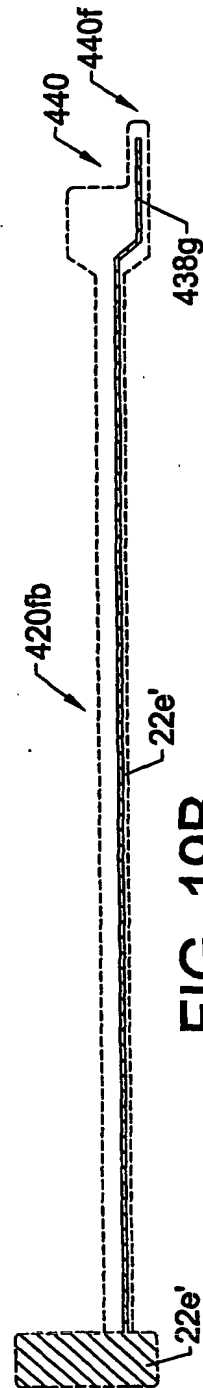
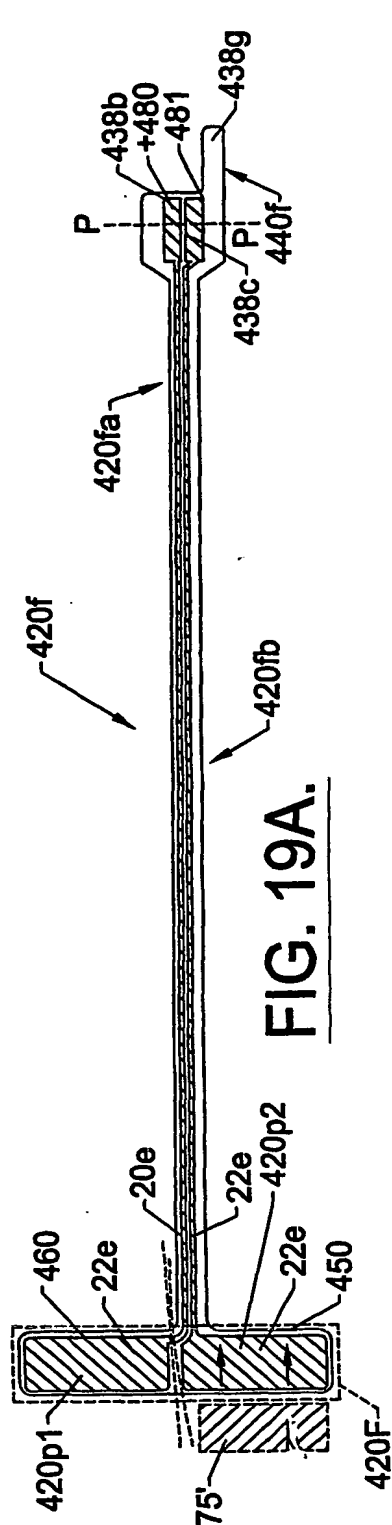


FIG. 18A.

18/30



FIG. 18B.



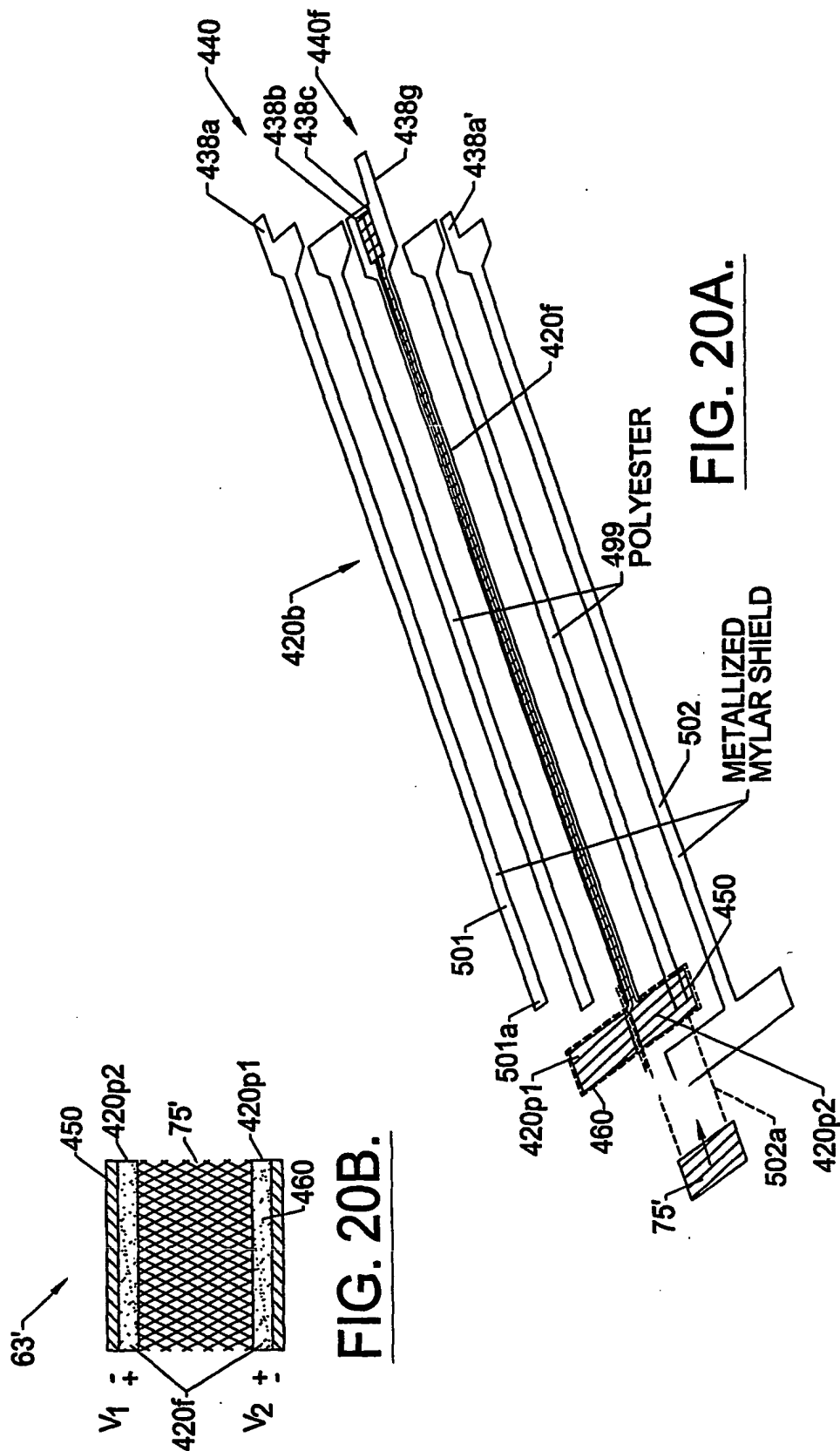


FIG. 20B.

FIG. 20A.

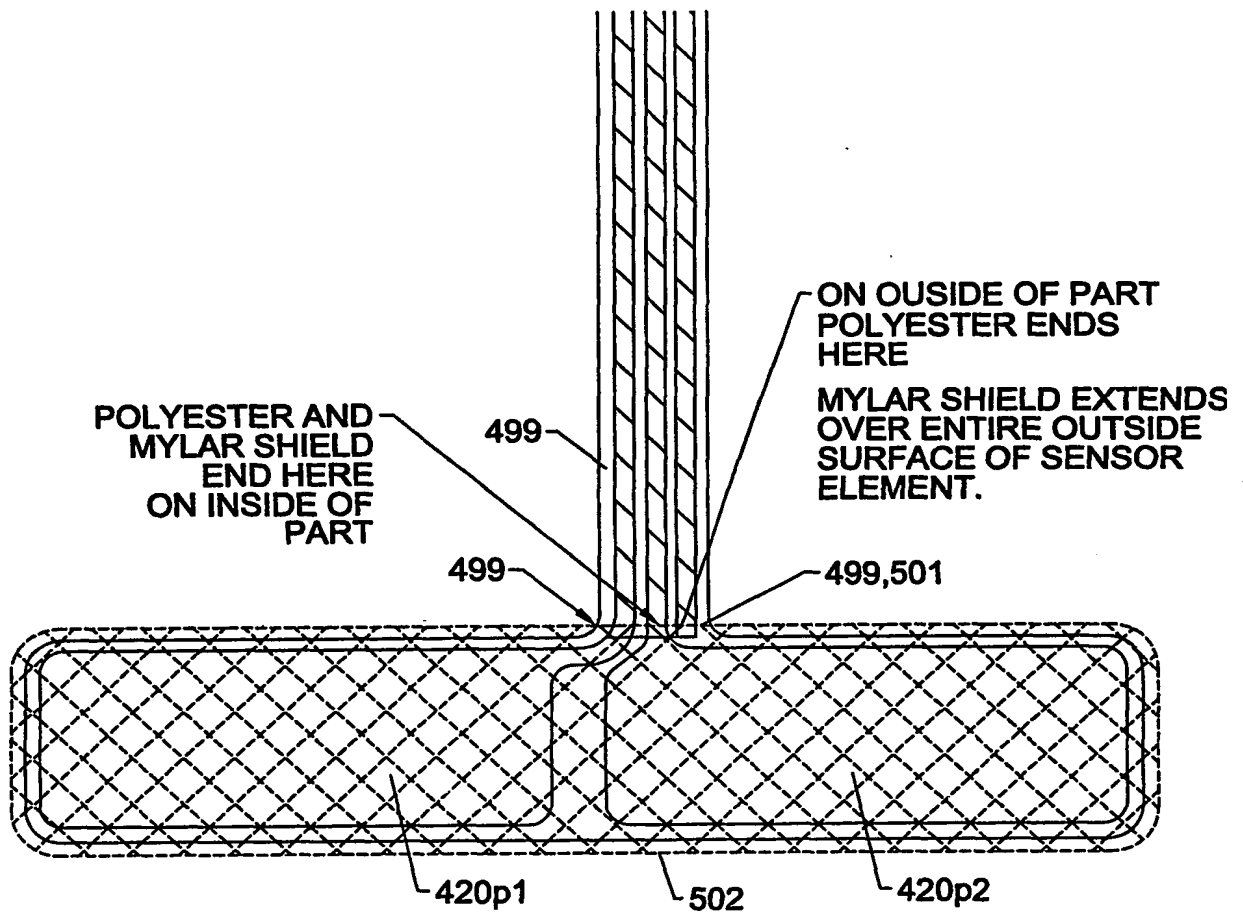
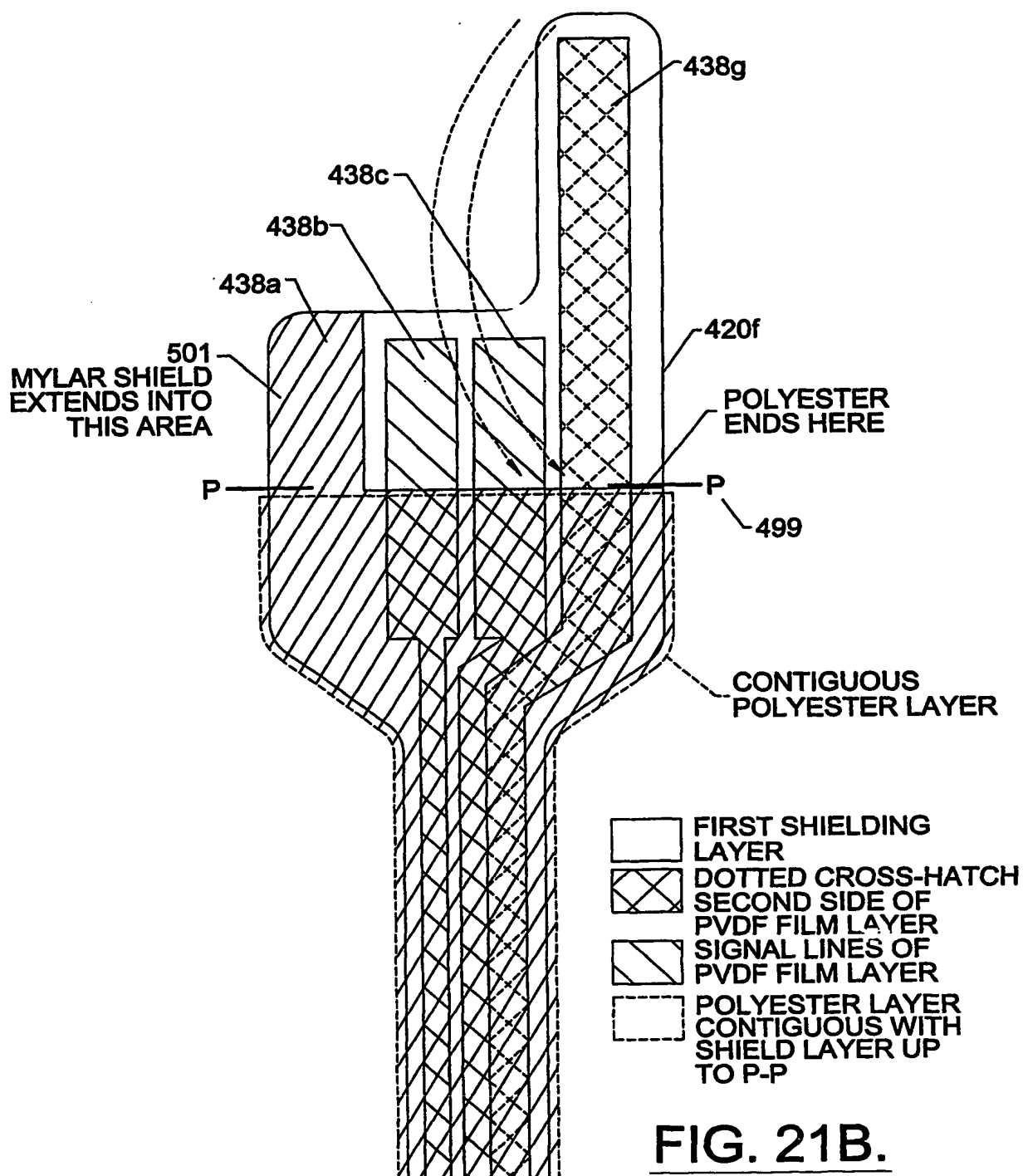
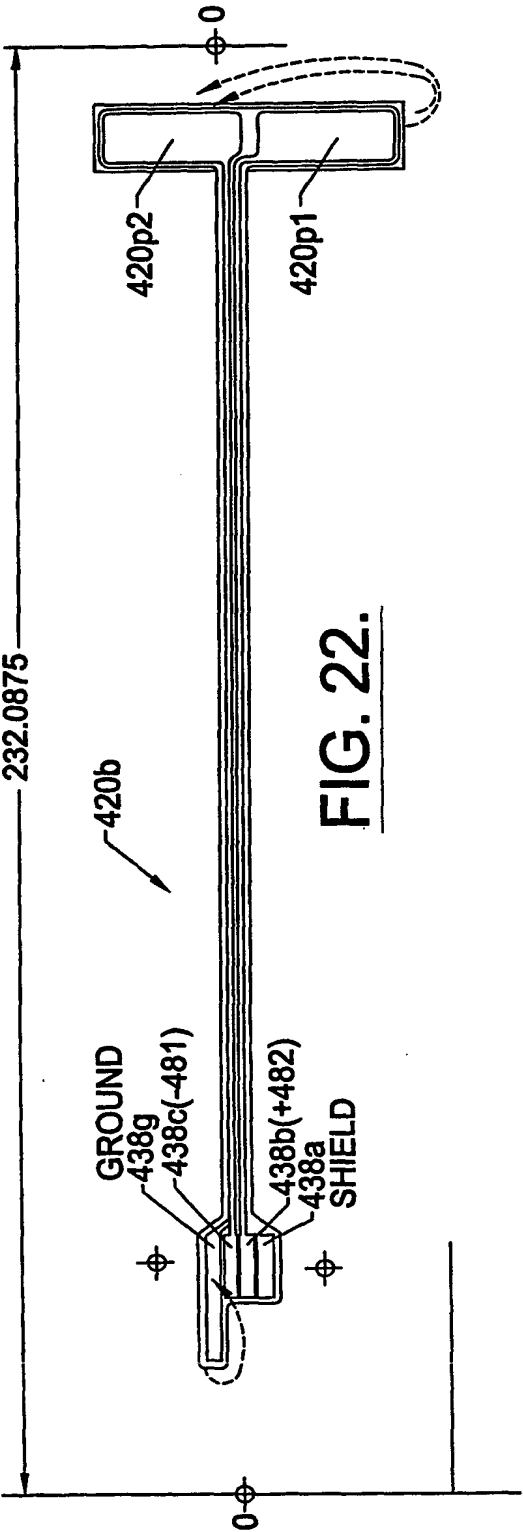


FIG. 21A.





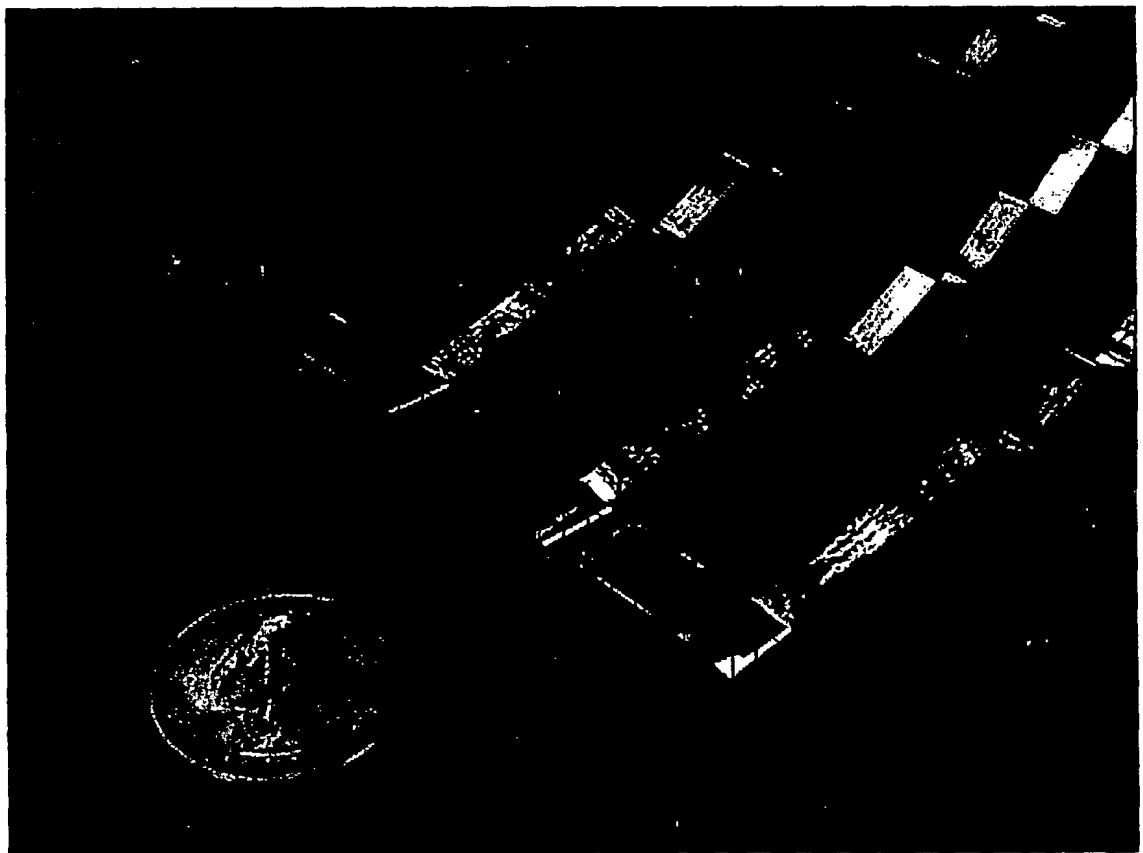


FIG. 23.

25/30



FIG. 24A.

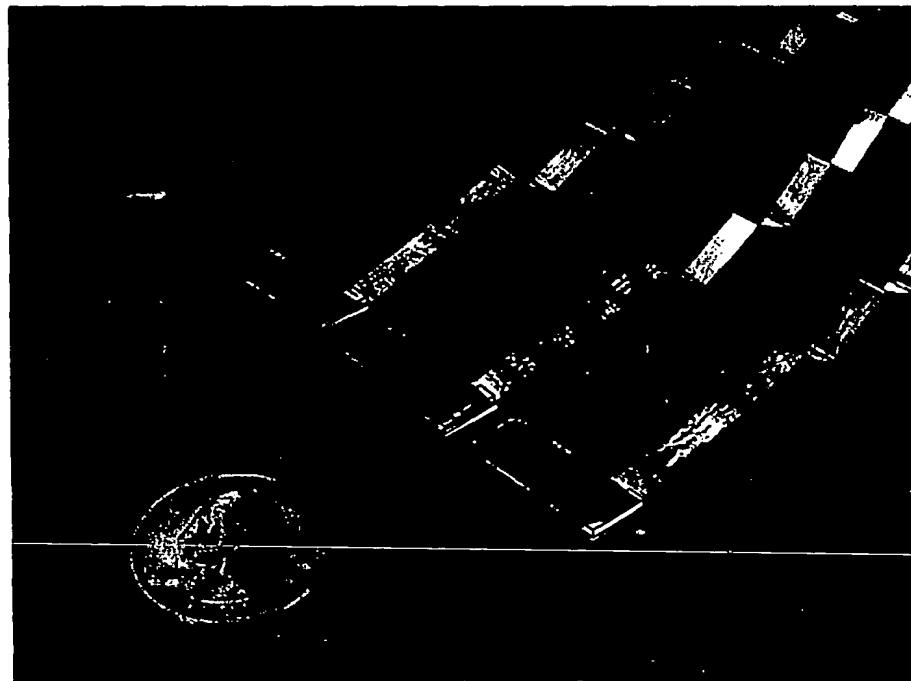


FIG. 24B.



FIG. 24C.

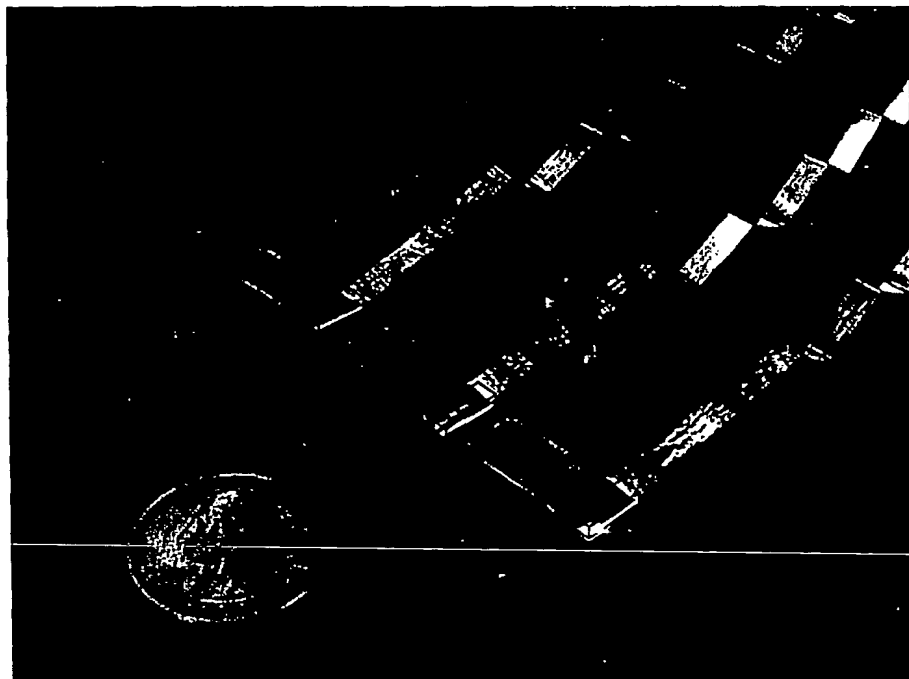


FIG. 24D.

27/30



FIG. 24E.

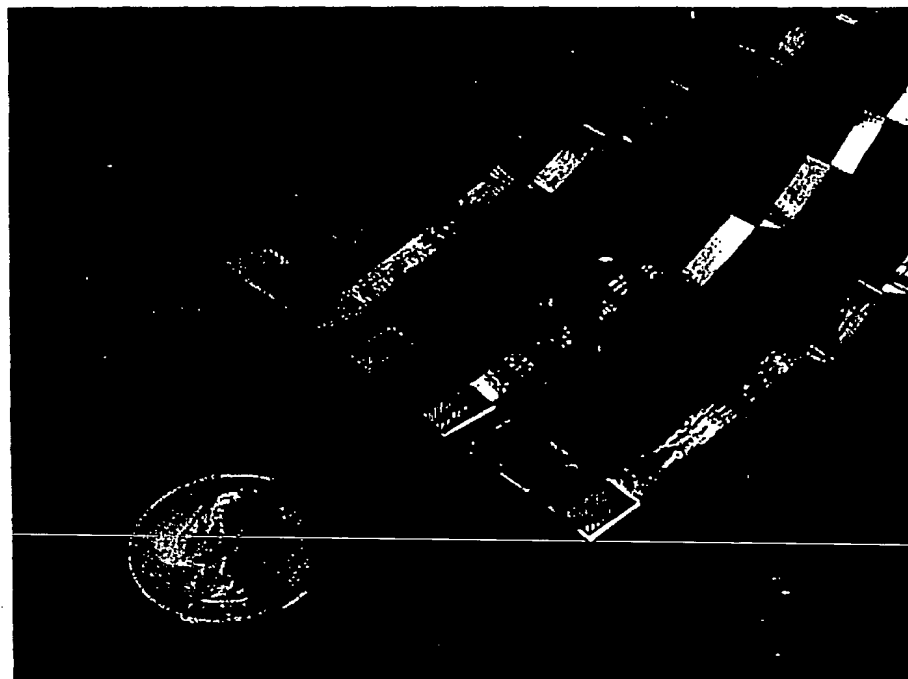


FIG. 25A.

28/30

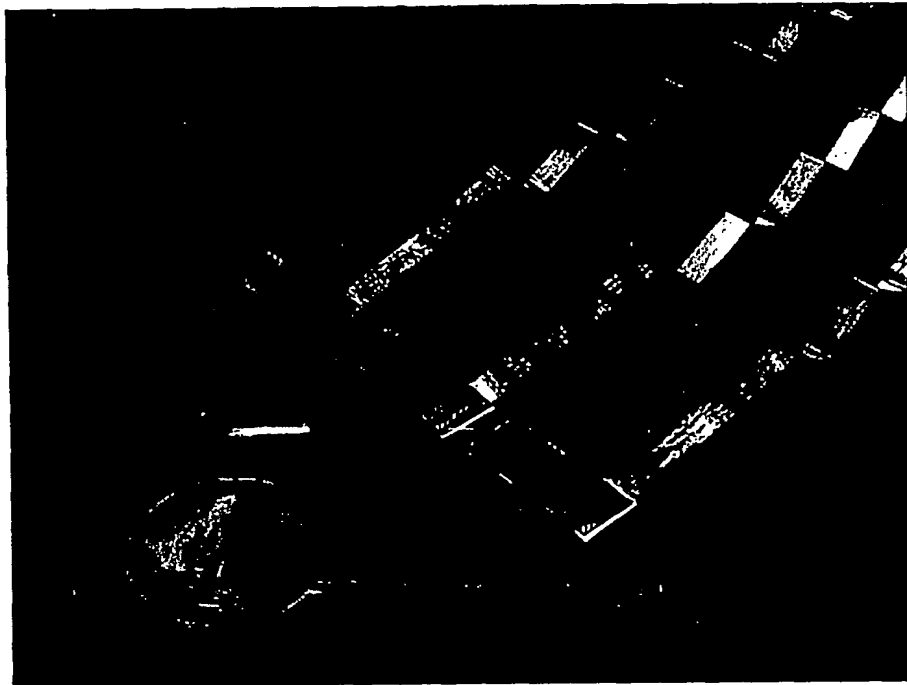


FIG. 25B.

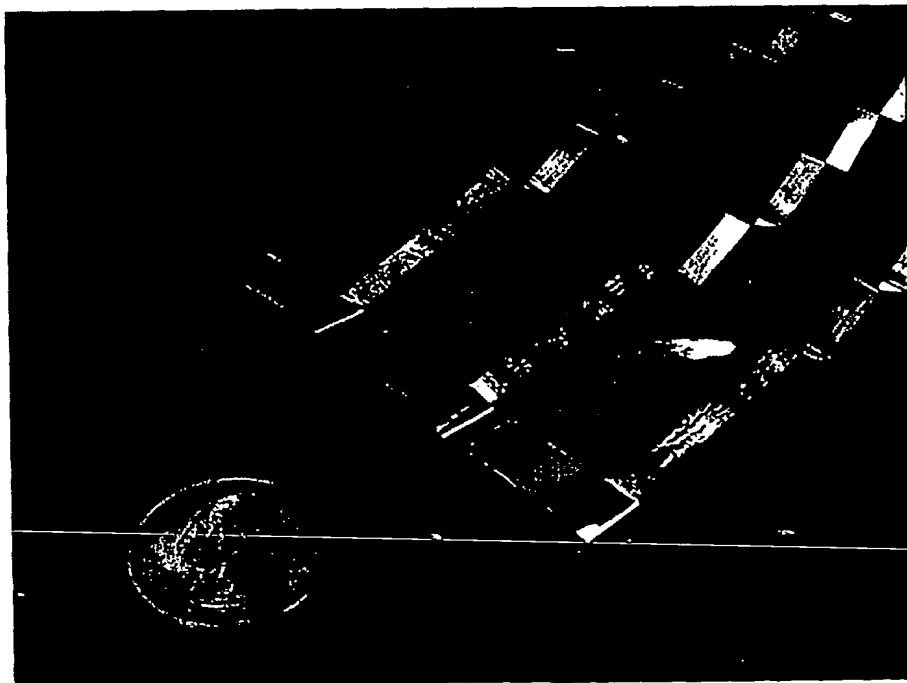


FIG. 25C.

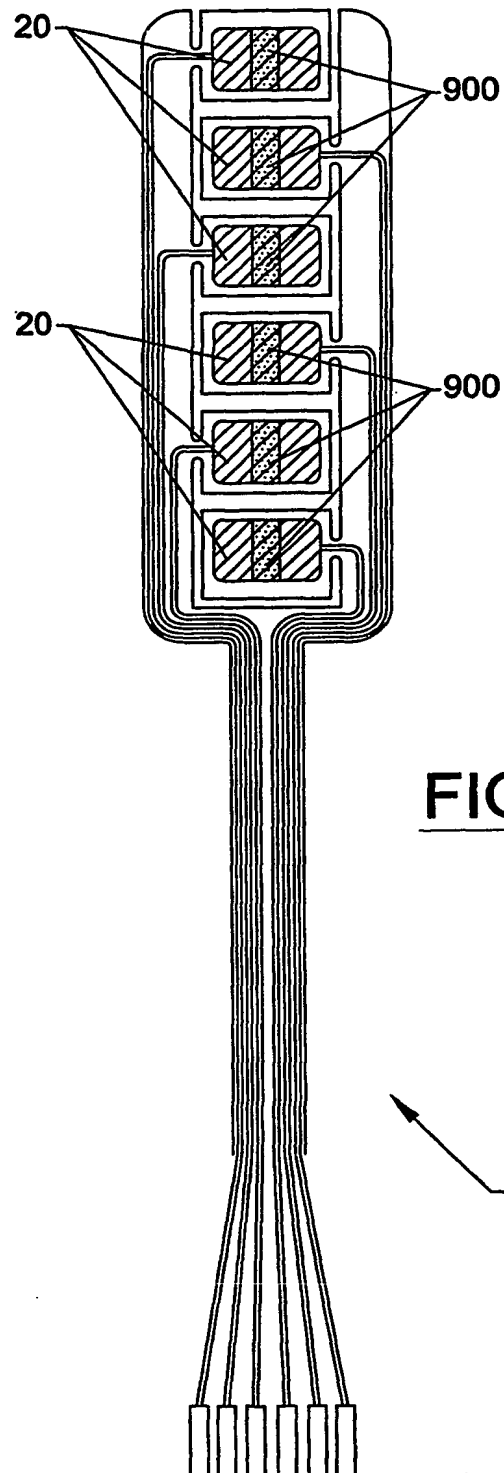
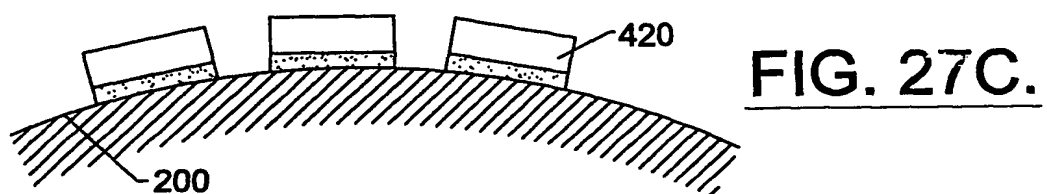
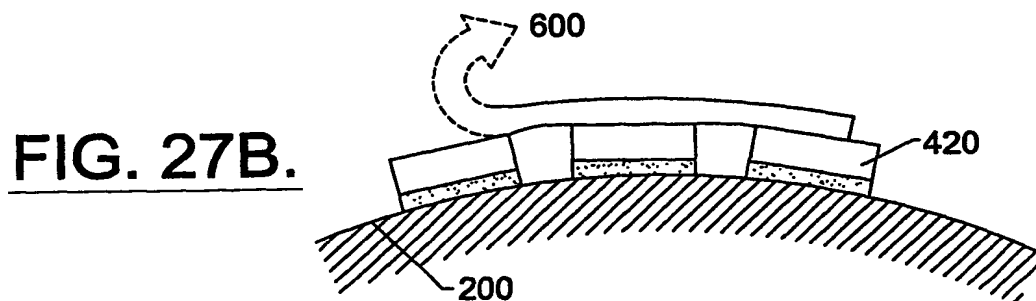
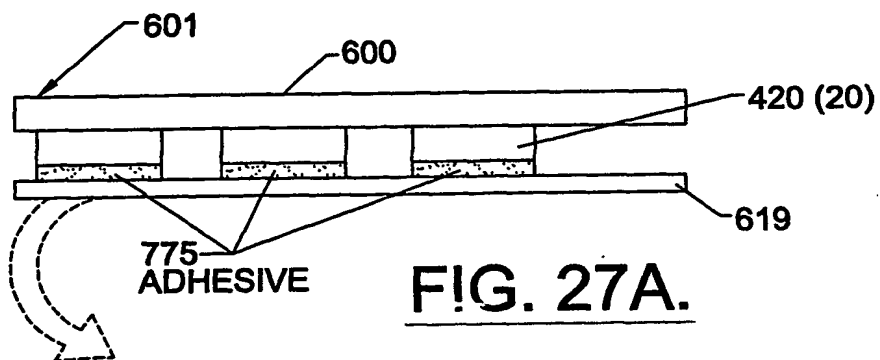


FIG. 26.



INTERNATIONAL SEARCH REPORT

International Application No

PC 00/05124

A. CLASSIFICATION OF SUBJECT MATTER
 IPC 7 B06B1/06 A61B7/04

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
 IPC 7 B06B A61B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO 98 22786 A (FLOWSCAN INC) 28 May 1998 (1998-05-28)	18-25
Y	page 1, line 1 - line 18 page 4, line 28 -page 7, line 28 page 11, line 37 -page 12, line 9 ---	1,44
Y	US 5 807 271 A (SOULUER FARID ET AL) 15 September 1998 (1998-09-15) column 1, line 5 - line 7 column 3, line 49 - line 58; claim 1; figure 3 ---	1,44
A	EP 0 420 190 A (ATOCHEM NORTH AMERICA) 3 April 1991 (1991-04-03) page 2, column 1, line 10 - line 15 page 4, column 5, line 45 -page 5, column 7, line 21 page 6, column 9, line 20 - line 45 --- -/--	1,18,37

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

* Special categories of cited documents :

- *A* document defining the general state of the art which is not considered to be of particular relevance
- *E* earlier document but published on or after the international filing date
- *L* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- *O* document referring to an oral disclosure, use, exhibition or other means
- *P* document published prior to the international filing date but later than the priority date claimed

T later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

X document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

Y document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

& document member of the same patent family

Date of the actual completion of the international search

27 September 2000

Date of mailing of the international search report

19.10.00

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2
 NL - 2280 HV Rijswijk
 Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
 Fax: (+31-70) 340-3016

Authorized officer

Lorne, B

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4 833 659 A (GEIL FREDERICK G ET AL) 23 May 1989 (1989-05-23) column 3, line 47 -column 4, line 23 column 6, line 37 -column 7, line 57 ---	1
A	WO 94 30030 A (UNIV CALIFORNIA) 22 December 1994 (1994-12-22) page 5, line 7 -page 8, line 24 ---	26
X	US 5 795 299 A (BRUMMER CHARLES W ET AL) 18 August 1998 (1998-08-18) column 1, line 49 -column 2, line 3 column 2, line 55 -column 3, line 13 column 4, line 16 - line 41; claim 1 ---	45-47,49
A	US 5 398 689 A (CONNOR BRIAN G ET AL) 21 March 1995 (1995-03-21) column 1, line 40 -column 2, line 26; claim 1 ---	66,68
A	US 5 680 863 A (COOPER THOMAS G ET AL) 28 October 1997 (1997-10-28) column 1, line 46 -column 2, line 31 ---	45
A	EP 0 801 927 A (MEDACOUSTICS INC) 22 October 1997 (1997-10-22) page 3, column 3, line 48 -column 4, line 24; claims 1,2 ---	57,70
A	US 5 598 845 A (STERN ROGER A ET AL) 4 February 1997 (1997-02-04) column 2, line 65 -column 3, line 8 column 4, line 1 - line 35; figures 2,3 ---	57,70
A	US 4 308 870 A (ARKANS EDWARD J) 5 January 1982 (1982-01-05) the whole document -----	57,70

INTERNATIONAL SEARCH REPORT

International application No.
PCT/US 00/05124

Box I Observations where certain claims were found unsearchable (Continuation of item 1 of first sheet)

This International Search Report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. ☐ Claims Nos.:
because they relate to subject matter not required to be searched by this Authority, namely:

2. ☐ Claims Nos.:
because they relate to parts of the International Application that do not comply with the prescribed requirements to such an extent that no meaningful International Search can be carried out, specifically:

3. ☐ Claims Nos.:
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

Box II Observations where unity of invention is lacking (Continuation of item 2 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

see additional sheet

1. ☒ As all required additional search fees were timely paid by the applicant, this International Search Report covers all searchable claims.

2. ☐ As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.

3. ☐ As only some of the required additional search fees were timely paid by the applicant, this International Search Report covers only those claims for which fees were paid, specifically claims Nos.:

4. ☐ No required additional search fees were timely paid by the applicant. Consequently, this International Search Report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest.
- ☒ No protest accompanied the payment of additional search fees.

FURTHER INFORMATION CONTINUED FROM PCT/ISA/ 210

This International Searching Authority found multiple (groups of) inventions in this international application, as follows:

1. Claims: 1-44

A low profile acoustic sensor array comprising strips with sensor elements mounted on frames with rails.

2. Claims: 45-56, 66-67, 68-69

Configuration of transmission lines with a series of undulations in the transmission paths.

3. Claims: 57-65, 70-73

A carrier member to hold the plurality of sensors.

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
WO 9822786 A	28-05-1998	US 5827198 A AU 4750397 A	27-10-1998 10-06-1998
US 5807271 A	15-09-1998	NONE	
EP 0420190 A	03-04-1991	US 5166573 A CA 2026053 A JP 3207200 A	24-11-1992 27-03-1991 10-09-1991
US 4833659 A	23-05-1989	NONE	
WO 9430030 A	22-12-1994	AU 6953994 A US 5633552 A US 5569968 A US 5728089 A	03-01-1995 27-05-1997 29-10-1996 17-03-1998
US 5795299 A	18-08-1998	NONE	
US 5398689 A	21-03-1995	DE 9402697 U JP 7008494 A	14-04-1994 13-01-1995
US 5680863 A	28-10-1997	US 5735282 A	07-04-1998
EP 0801927 A	22-10-1997	US 5365937 A AU 5099693 A CA 2144169 A DE 69323085 D DE 69323085 T EP 0659058 A WO 9405207 A US 5807268 A US 5913829 A	22-11-1994 29-03-1994 17-03-1994 25-02-1999 24-06-1999 28-06-1995 17-03-1994 15-09-1998 22-06-1999
US 5598845 A	04-02-1997	AU 717213 B AU 7599996 A CA 2237967 A EP 0862381 A WO 9717883 A	23-03-2000 05-06-1997 22-05-1997 09-09-1998 22-05-1997
US 4308870 A	05-01-1982	CA 1166701 A	01-05-1984

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
21 September 2000 (21.09.2000)

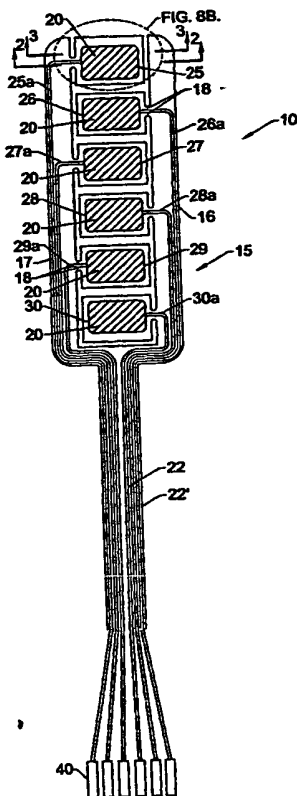
PCT

(10) International Publication Number
WO 00/54897 A3

- (51) International Patent Classification⁷: B06B 1/06, (72) Inventors; and
A61B 7/04 (75) Inventors/Applicants (for US only): SLEVA, Michael, Z. [US/US]; 6608 Rocky Falls Road, Charlotte, NC 28211 (US). EBERHARDT, Allen [US/US]; 624 Marlowe Road, Raleigh, NC 27609 (US). SWANSON, Cal [US/US]; 1626 Shepherds Glade Drive, Apex, NC 27502 (US). TRIOLO, Richard [US/US]; 6021 Apt. E Shadowtree Lane, Raleigh, NC 27613 (US). LEWANDOWSKI, Simon [US/US]; 6313 Lynn Meadow Drive, Raleigh, NC 27609 (US).
- (21) International Application Number: PCT/US00/05124
- (22) International Filing Date: 29 February 2000 (29.02.2000)
- (25) Filing Language: English
- (26) Publication Language: English
- (30) Priority Data:
60/122,264 1 March 1999 (01.03.1999) US
60/132,041 30 April 1999 (30.04.1999) US
- (71) Applicant (for all designated States except US): MEDA-
COUSTICS, INC. [US/US]; Suite 114, 5540 Centerview
Drive, Raleigh, NC 27606 (US).
- (74) Agents: RICHARDSON, Julie, H. et al.; Myers, Bigel,
Sibley & Sajovec, P.A., P.O. Box 37428, Raleigh, NC
27627 (US).
- (81) Designated States (national): AE, AL, AM, AT, AT (util-
ity model), AU, AZ, BA, BB, BG, BR, BY, CA, CH, CN,
CU, CZ, CZ (utility model), DE, DE (utility model), DK,
DK (utility model), EE, EE (utility model), ES, FI, FI (util-
ity model), GB, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP,

[Continued on next page]

(54) Title: LOW PROFILE ACOUSTIC SENSOR ARRAY AND SENSORS WITH PLEATED TRANSMISSION LINES AND RELATED METHODS



(57) Abstract: A low profile acoustic array (10) is configured to selectively respond to shear waves while rejecting compression wave energy in the frequency range of interest. One sensor array is configured as a linear strip with a frame segment having at least one longitudinally extending rail and a plurality of sensor elements (20) extending therefrom. These sensor elements have a resilient core and opposing PDVF outer layers configured with opposing polarities onto the core. The linear strip array also includes a pair of separate electrical signal transmission paths. The transmission lines can include a series of undulations formed thereon to help minimize undesired mechanical crossover between sensors. A carrier member can be configured to be detachably releasable carries the discrete sensors to maintain the positional alignment until they are secured to a patient.

WO 00/54897 A3



KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SK (utility model), SL, TJ, TM, TR, TT, UA, UG, US, UZ, VN, YU, ZA, ZW.

- (84) **Designated States (regional):** ARIPO patent (GH, GM, KE, LS, MW, SD, SL, SZ, TZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG).

Published:

— with international search report

- (88) **Date of publication of the international search report:**
26 July 2001

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

INTERNATIONAL SEARCH REPORT

International Application No

PC., JS 00/05124

A. CLASSIFICATION OF SUBJECT MATTER
 IPC 7 B06B1/06 A61B7/04

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 B06B A61B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO 98 22786 A (FLOWSCAN INC) 28 May 1998 (1998-05-28)	18-25
Y	page 1, line 1 - line 18 page 4, line 28 -page 7, line 28 page 11, line 37 -page 12, line 9 ---	1,44
Y	US 5 807 271 A (SOULUER FARID ET AL) 15 September 1998 (1998-09-15) column 1, line 5 - line 7 column 3, line 49 - line 58; claim 1; figure 3 ---	1,44
A	EP 0 420 190 A (ATOCHEM NORTH AMERICA) 3 April 1991 (1991-04-03) page 2, column 1, line 10 - line 15 page 4, column 5, line 45 -page 5, column 7, line 21 page 6, column 9, line 20 - line 45 --- -/--	1,18,37

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

* Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier document but published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

"&" document member of the same patent family

Date of the actual completion of the international search

27 September 2000

Date of mailing of the international search report

19.10.00

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2
 NL - 2280 HV Rijswijk
 Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
 Fax: (+31-70) 340-3016

Authorized officer

Lorne, B

INTERNATIONAL SEARCH REPORT

International Application No.

PC./JS 00/05124

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4 833 659 A (GEIL FREDERICK G ET AL) 23 May 1989 (1989-05-23) column 3, line 47 -column 4, line 23 column 6, line 37 -column 7, line 57 ---	1
A	WO 94 30030 A (UNIV CALIFORNIA) 22 December 1994 (1994-12-22) page 5, line 7 -page 8, line 24 ---	26
X	US 5 795 299 A (BRUMMER CHARLES W ET AL) 18 August 1998 (1998-08-18) column 1, line 49 -column 2, line 3 column 2, line 55 -column 3, line 13 column 4, line 16 - line 41; claim 1 ---	45-47,49
A	US 5 398 689 A (CONNOR BRIAN G ET AL) 21 March 1995 (1995-03-21) column 1, line 40 -column 2, line 26; claim 1 ---	66,68
A	US 5 680 863 A (COOPER THOMAS G ET AL) 28 October 1997 (1997-10-28) column 1, line 46 -column 2, line 31 ---	45
A	EP 0 801 927 A (MEDACOUSTICS INC) 22 October 1997 (1997-10-22) page 3, column 3, line 48 -column 4, line 24; claims 1,2 ---	57,70
A	US 5 598 845 A (STERN ROGER A ET AL) 4 February 1997 (1997-02-04) column 2, line 65 -column 3, line 8 column 4, line 1 - line 35; figures 2,3 ---	57,70
A	US 4 308 870 A (ARKANS EDWARD J) 5 January 1982 (1982-01-05) the whole document -----	57,70

INTERNATIONAL SEARCH REPORT

International application No.
PCT/US 00/05124

Box I Observations where certain claims were found unsearchable (Continuation of item 1 of first sheet)

This International Search Report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. ☐ Claims Nos.:
because they relate to subject matter not required to be searched by this Authority, namely:
2. ☐ Claims Nos.:
because they relate to parts of the International Application that do not comply with the prescribed requirements to such an extent that no meaningful International Search can be carried out, specifically:
3. ☐ Claims Nos.:
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

Box II Observations where unity of invention is lacking (Continuation of item 2 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

see additional sheet

1. ☒ As all required additional search fees were timely paid by the applicant, this International Search Report covers all searchable claims.
2. ☐ As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.
3. ☐ As only some of the required additional search fees were timely paid by the applicant, this International Search Report covers only those claims for which fees were paid, specifically claims Nos.:
4. ☐ No required additional search fees were timely paid by the applicant. Consequently, this International Search Report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest.
- ☒ No protest accompanied the payment of additional search fees.

FURTHER INFORMATION CONTINUED FROM PCT/ISA/ 210

This International Searching Authority found multiple (groups of) inventions in this international application, as follows:

1. Claims: 1-44

A low profile acoustic sensor array comprising strips with sensor elements mounted on frames with rails.

2. Claims: 45-56, 66-67, 68-69

Configuration of transmission lines with a series of undulations in the transmission paths.

3. Claims: 57-65, 70-73

A carrier member to hold the plurality of sensors.

INTERNATIONAL SEARCH REPORT

- automatic patent family members

International Application No

PC, JS 00/05124

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
WO 9822786	A	28-05-1998	US 5827198 A	27-10-1998
			AU 4750397 A	10-06-1998

US 5807271	A	15-09-1998	NONE	

EP 0420190	A	03-04-1991	US 5166573 A	24-11-1992
			CA 2026053 A	27-03-1991
			JP 3207200 A	10-09-1991

US 4833659	A	23-05-1989	NONE	

WO 9430030	A	22-12-1994	AU 6953994 A	03-01-1995
			US 5633552 A	27-05-1997
			US 5569968 A	29-10-1996
			US 5728089 A	17-03-1998

US 5795299	A	18-08-1998	NONE	

US 5398689	A	21-03-1995	DE 9402697 U	14-04-1994
			JP 7008494 A	13-01-1995

US 5680863	A	28-10-1997	US 5735282 A	07-04-1998

EP 0801927	A	22-10-1997	US 5365937 A	22-11-1994
			AU 5099693 A	29-03-1994
			CA 2144169 A	17-03-1994
			DE 69323085 D	25-02-1999
			DE 69323085 T	24-06-1999
			EP 0659058 A	28-06-1995
			WO 9405207 A	17-03-1994
			US 5807268 A	15-09-1998
			US 5913829 A	22-06-1999

US 5598845	A	04-02-1997	AU 717213 B	23-03-2000
			AU 7599996 A	05-06-1997
			CA 2237967 A	22-05-1997
			EP 0862381 A	09-09-1998
			WO 9717883 A	22-05-1997

US 4308870	A	05-01-1982	CA 1166701 A	01-05-1984
